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3 1 **FLUID FLOW SIMULATION AND PERMEABILITY COMPUTATION IN DEFORMED**
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5 2 **POROUS CARBONATE GRAINSTONES**
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29 15 **Abstract**
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31 16 In deformed porous carbonates, the architecture of the pore network may be modified by
32 17 deformation or diagenetic processes varying the permeability with respect to the pristine rock. The
33 18 effects of the pore texture and morphology on permeability in porous rocks have been widely
34 19 investigated due to the importance during the evaluation of geofluids reservoirs. In this study, these
35 20 effects are assessed by combining synchrotron X-ray computed microtomography (SR micro-CT)
36 21 and computational fluid dynamics. The studied samples pertain to deformed porous carbonate
37 22 grainstones highly affected by deformation bands (DBs) exposed in Northwestern Sicily and Abruzzo
38 23 regions, Italy.
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40 24 The high-resolution SR micro-CT images of the samples, acquired at the SYRMEP beamline
41 25 of the Elettra - Sincrotrone Trieste laboratory (Italy), were used for simulating a pressure-driven flow
42 26 by using the lattice-Boltzmann method (LBM). For the experiments, a multiple relaxation time (MRT)
43 27 model with the D3Q19 scheme was used to avoid viscosity-dependent results of permeability. The
44 28 permeability was calculated by using the Darcy's law once steady conditions were reached. After the
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63 29 simulations, the pore-network properties (porosity, specific surface area, and geometrical tortuosity)
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65 30 were calculated using the lattice velocity 3D images. Which were segmented considering a velocity
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67 31 threshold value higher than zero.

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70 32 The study showed that DBs represents important heterogeneity features which generate
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72 33 significant permeability anisotropy. Cataclasis and cementation process taking place within the DBs
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74 34 reduce the effective porosity and therefore the permeability. Contrary, pressure dissolution and
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76 35 faulting may generate connected channels which contribute to the permeability only parallel to the
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78 36 DB.

80 37 Keywords: *Deformation bands; tortuosity; porosity; synchrotron X-ray computed microtomography;*
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82 38 *lattice-Boltzmann Method.*
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84 39
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87 40 **Highlights:**

- 89 41 • An MRT-LBM was used for obtaining viscosity-independent permeability in deformed
90 42 carbonates.
- 92 43 • The influence of the pore-network morphology on the permeability was investigated.
- 94 44 • Fault core shows important heterogeneity and permeability anisotropy in comparison to the
95 45 host rock.

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1. Introduction

During the evaluation and development of geofluid reservoirs (water or hydrocarbons), one of the most elusive aspects is obtaining relationships between porosity and permeability. The permeability-porosity cross plots typically show important variability, which may indicate that permeability depends not only on the porosity but also on textural and hydraulic properties of the pore network such as pores size distribution, pores shape, and tortuosity (Carman, 1937; Dullien, 1992; Lucia, 2007).

Different attempts have been made to relate the pore-network properties and the permeability in order to describe their control or estimate the value of permeability (e.g. Kozeny, 1927; Carman, 1937; Archie, 1942; Wyllie and Rose, 1950; Swanson, 1981; and Katz and Thompson, 1986). One of the most widely used indirect methods for estimating the permeability is based on the so-called Kozeny-Carman (K-C) equation (Kozeny, 1927; Carman, 1937):

$$k = \frac{\phi^3}{\beta \tau^2 S^2} \quad (\text{equation 1})$$

Where ϕ is the effective porosity, S is the specific surface area (depending on grain size and texture), τ is the tortuosity (here defined as the ratio of the actual length of fluid path divided by the Euclidean distance), and β is a pore shape factor normally rounded to 5.

The K-C equation is widely applied to estimate the permeability of realistic rock samples (e.g. Cerepi *et al.*, 2001; Agosta *et al.*, 2007) or fictitious rocks (Adler *et al.*, 1990). Adler *et al.* (1990) described the flow in complex pore geometries in modelled porous media based on statistical analysis thin section of homogeneous sandstones. These authors also found that the permeability values estimated with the Kozeny-Carman equation was significantly lower than permeability measured in laboratory. According to Dullien (1992), the K-C equation is often not valid in the following cases: i) when grains strongly deviate from the spherical shape, ii) when grains show a broad size distribution, or ii) when the grains are consolidated. Therefore, the K-C equation may be not valid for instance to estimate the permeability in deformed or diagenetic carbonates. A possible source of

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183 72 error in the implementation of the K-C equation is that its variables are often indirectly measured
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185 73 (Dullien, 1992; Wildenschild and Sheppard, 2013).

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187 74 The direct flow simulations are currently widely used to calculate single phase flow and
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189 75 transport in complex porous media (Blunt *et al.*, 2013; Bultreys *et al.*, 2016, and references therein).
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191 76 Transport in rocks have been studied directly on realistic 3D pore space (obtained by X-ray
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193 77 tomographic, nuclear magnetic resonance), on reconstructed models from 2-D thin section images,
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195 78 and fictitious models. The three classical computational fluid dynamics approaches used for
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197 79 simulating fluid flow in porous media are: i) the finite difference method (Stapf *et al.*, 2000; Øren
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199 80 and Bakke, 2002; Bijeljic *et al.*, 2011; Mostaghimi *et al.*, 2012; Bijeljic *et al.*, 2013; Blunt *et al.*,
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201 81 2013), ii) the finite element method (Cardenas, 2008, 2009; Mostaghimi *et al.*, 2013), and iii) the
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203 82 finite volume method (Zhang *et al.*, 2012; Peng *et al.*, 2014). In addition to these techniques, the
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205 83 lattice-Boltzmann method (LBM) is widely used for modeling flow in complex geometries
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207 84 (Dunsmuir *et al.*, 1991; Chen and Doolen, 1998; Manz *et al.*, 1999; Kang *et al.*, 2006; Manwart *et al.*,
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209 85 2002; Sukop *et al.*, 2008; Porter *et al.*, 2009; Schaap *et al.*, 2007; Pan *et al.*, 2004; Pan *et al.*, 2006;
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211 86 Hao and Cheng, 2010; Boek and Venturoli, 2010; Landry *et al.*, 2014; Yang *et al.*, 2016).

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213 87 The LBM describes the flow of a large number of particles interacting with the medium and
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215 88 among themselves following the Navier-Stokes equation at the macroscopic scale (Ladd, 1994). The
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217 89 LBM can handle complex pore geometry without any simplification and accurately describes fluid
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219 90 flow in porous media (Ladd, 1994; Keehm *et al.*, 2001). Pan *et al.* (2006) quantitatively evaluated the
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221 91 capability and accuracy of the LBM for modeling flow through two porous media, a body-centered
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223 92 cubic array of spheres and a random-sized sphere-pack. Yang *et al.* (2016) applied LBM and three
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225 93 other approaches (standard finite volume method, smoothed particle hydrodynamics, pore-network
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227 94 model) to simulate pore-scale velocity distributions and nonreactive solute transport. Sukop *et al.*
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229 95 (2008) used a parallel implementation of the three-dimensional Shan-and-Chen multicomponent,
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231 96 multiphase LBM to simulate the equilibrium distributions of two immiscible fluids in a quartz sand
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233 97 porous medium using cone-beam X-ray microtomography.
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243 98 The LBM have been used to study the permeability on 3D images of rocks and soft sediments,
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245 99 obtained by micro-CT imaging techniques (Andrä *et al.*, 2013; Fredrich *et al.*, 2006; Khan *et al.*,
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247 100 2012; Manwart *et al.*, 2002; Li *et al.*, 2005; Degruyter *et al.*, 2010; Shah *et al.*, 2015) and from
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249 reconstructed models (Jin *et al.*, 2004; Keehm, 2004; Wu *et al.*, 2006). The computed permeability
250 101 using the LBM has shown a good agreement with laboratory measurements over a wide range of
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252 102 permeability values (Keehm *et al.*, 2003, 2004). Manwart *et al.* (2002) compared the finite difference
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254 103 and the lattice Boltzmann approaches for calculating the permeability. These authors showed that the
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256 104 computation times and numerical results of the two methods were similar, however LBM is more
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258 105 memory demanding.
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262 107 The simplest LBM is based on the Bhatnagar-Gross-Krook (BGK) collision operator, which
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264 108 consists in a single relaxation time approximation (Bhatnagar *et al.*, 1954). Using three-dimensional
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266 109 (3D) images at high spatial resolution collected at different synchrotron facilities, Degruyter *et al.*
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268 (2010) performed single phase gas simulations with the BGK-LBM and estimated the permeability
269 110 in volcanic rocks by means of the software PALABOS (Latt, 2009). Ahrenholz *et al.* (2008) used the
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271 111 BGK-LBM to solve the coupled Navier–Stokes equations for two phases, to describe the dynamics
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273 112 of the fluid/fluid interface and to predict capillary hysteresis in a porous sand imaged with X-ray
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275 113 tomography. Despite its popularity, the BGK-LBM presents some drawbacks, for instance, the
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277 114 obtained permeability may be viscosity-dependent (Narvaez *et al.*, 2010). A more accurate alternative
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279 115 is the implementation of multiple relaxation times (MRT) methods, which are more stable and solve
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281 116 the drawbacks of the BGK method (e.g. d’Humières, 1992; d’Humières, *et al.* 2002). Pan *et al.* (2006)
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283 demonstrated that the MRT–LBM is superior to the BGK–LBM, and interpolation significantly
284 117 improves the accuracy of the fluid–solid boundary conditions. MRT-LBM could be useful to
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286 118 implement experiments of multiple-phase flows. Zhang *et al.* (2016) used multi-relaxation time
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288 119 MRT-LBM to study the effect of the geometrical characteristics of bi-dimensional (2D) artificial
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290 120 porous media on the relative permeability in immiscible two-phase flows.
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303 123 This work attempts to provide more evidence concerning the control exerted by the effective
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305 124 porosity, specific surface area and tortuosity on permeability in deformed carbonate rocks. This
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308 125 objective has been reached by combining quantitative images analysis and computational fluid
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310 126 dynamics using synchrotron radiation computed microtomography (SR micro-CT) images of
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312 127 deformed carbonate rock samples. The SR micro-CT images were acquired at the Elettra -
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314 128 Sincrotrone Trieste laboratory (Basovizza, Italy) and processed and analyzed as described by
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316 129 Zambrano *et al.* (2017). Due to the heterogeneity of the studied samples, different volumes of interest,
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318 130 containing pristine, deformed and diagenetized rocks, are analyzed to evaluate the effect of
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320 131 deformation on permeability. The permeability of deformed porous carbonate rocks was estimated
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322 132 via LBM, using the PALABOS open source library (Latt, 2009). The method and the code have been
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324 133 modified with respect to the work of Degruyter *et al.* (2010): the application of the MRT approach
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327 134 has been adopt in the present study rather than the BGK one in order to assure that values of
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329 135 permeability are viscosity-independent.
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2. Methodology

2.1. Rock samples description

The samples selected for this study are from outcrops located in Sicily, southern Italy (Favignana Island and San Vito Lo Capo Peninsula; Fig. 1a, c) and Abruzzo Region, central Italy (Maiella Mt.; Fig. 1b, d), hereafter called San Vito Lo Capo Grainstone (SVG), Favignana Island Grainstone (FIG), and Orfento Fm. Grainstone (OFG), respectively. The studied rocks are different in terms of the grain composition, age and burial history. The SVGs (Early Pleistocene in age) are poor-to-medium consolidated grainstones with grains made up of fragments of carbonates, marls, and shales with a diameter between 0.05 and 1.0 mm. The matrix, about 22% of the rock volume, is composed of bladed and sparry calcite cement with carbonate and marl fragments smaller than 0.05 mm (Tondi, 2007). The Early Pleistocene FIGs consist of well-preserved bioclasts composed of *Vermetus*, *Serpula*, bivalves, echinoids, red algae and corals ranging in size from submillimeter to centimeter (Tondi *et al.*, 2012). The host rock is poorly cemented with the cement limited to the grain contacts, around echinoids, or within intragranular pores (Tondi *et al.*, 2012). The OFGs (Campanian to Maastrichtian in age) are composed of fragments of rudists (Mutti, 1995). The OFG experienced a maximum burial depth between 0.5 and 3 km (Ori *et al.*, 1986; Graham *et al.*, 2003; Rustichelli *et al.*, 2016), while both SVG and FIG experienced a shallower maximum burial depth of approximated 30 m (Tondi *et al.*, 2012; Antonellini *et al.*, 2014).

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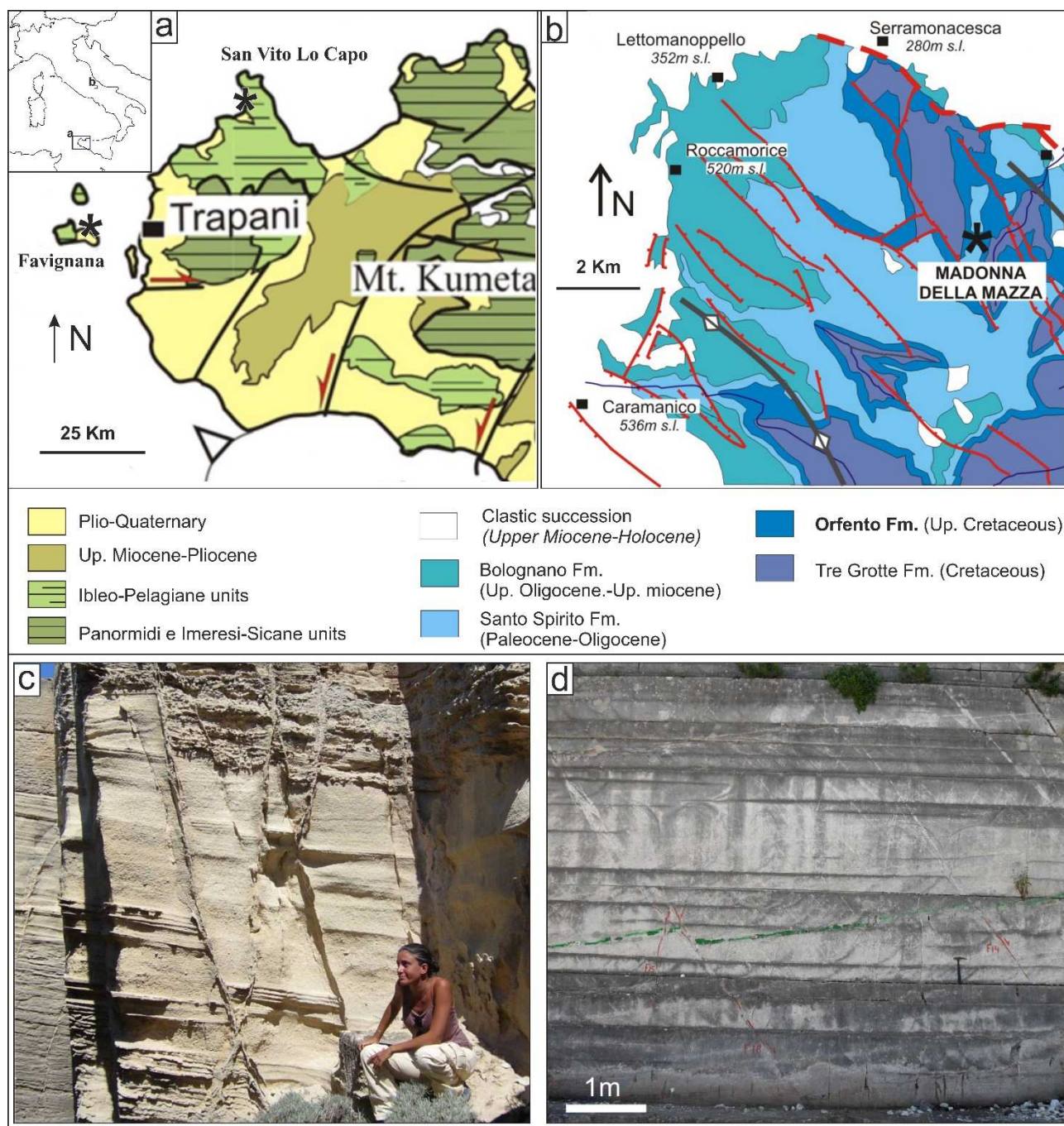


Figure 1. - Geological maps and location of the studied outcrops of a) Favignana Island and San Vito Lo Capo peninsula, and b) the northern part of the Maiella Mountain (modified from Tondi *et al.*, 2016). Outcrop images of the studied rocks showing both c) FIG and d) OFG crosscut by normal faults and compressive shear bands.

The studied samples may contain deformation bands (DBs), where strain localization (Aydin, 1978; Antonellini *et al.*, 1994; Fossen *et al.*, 2007; Cilona *et al.*, 2012, 2014) and chemical processes such as pressure solution and cementation (Hellman *et al.*, 2002; Tondi *et al.*, 2006; Tondi, 2007; Gaviglio *et al.*, 2009) may take place. Tondi *et al.* (2006) defined three diagenetic/structural tabular zones within the DBs (Zones I, II, III; Fig. 2) with different textures. Zones I and II are defined as the

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fault core of the deformation band (Tondi, 2007). Zone I (ZI), located at the inner part of the DB, includes the slip surfaces and a well-developed continuous zone of grain size and porosity reduction. Zone II (ZII), which limits the ZI, is a compacted grain zone characterized by pressure dissolution at the grain contacts. Zone III (ZIII) surrounds the fault core and is characterized by porosity reduction due to precipitation of calcite cement. Within DBs, the porosity and permeability are reduced considerably likely buffering for geofluid migration (Fossen and Bale, 2007; Tondi, 2007; Antonellini *et al.*, 2014; Tondi *et al.*, 2016).

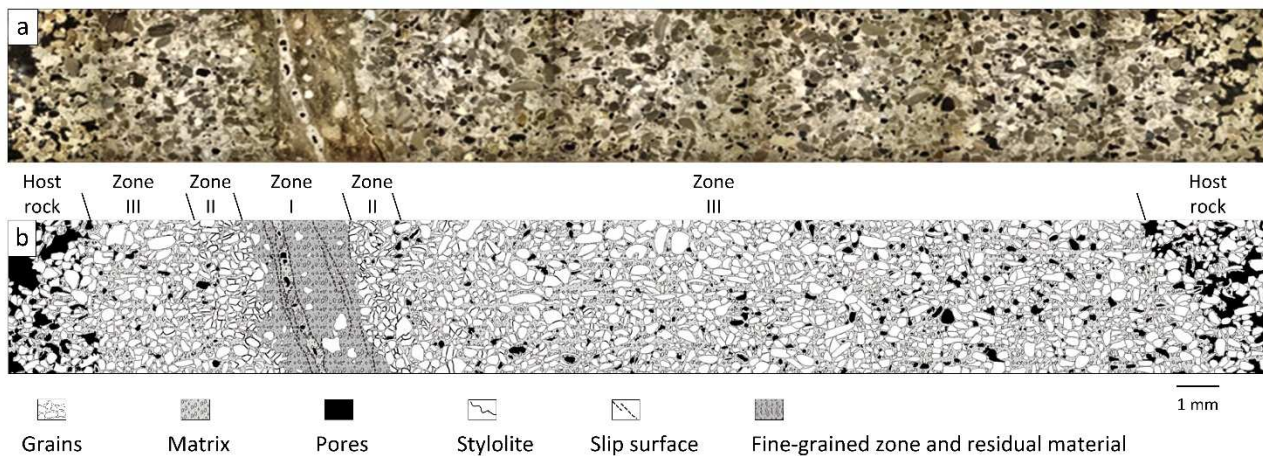
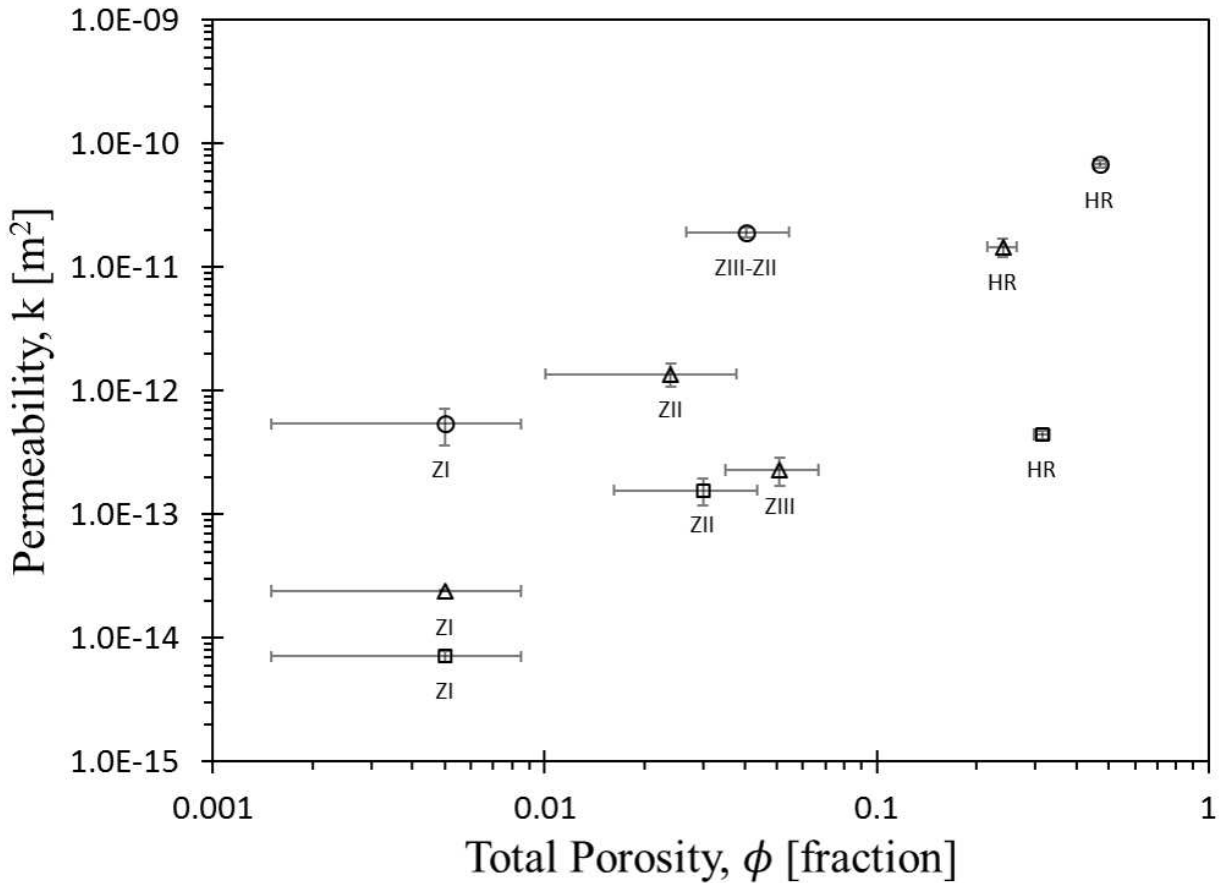


Figure 2. – Single deformation band from San Vito Lo Capo grainstone characterized by tabular zones (Zones I, II, and III) with different textures (see text for description) enclosed by the host rock; (a) microphotographs and (b) interpretation (after Tondi, 2007).

The permeability of the studied rocks has been previously assessed by Antonellini *et al.* (2014) and Tondi *et al.* (2016) in both host rock and DBs (including Zones I, II and III) using a TinyPerm II Portable Air permeameter (with a reliable range of 10^{-17} to 10^{-12} m²). The surface was carefully cleaned and a silicon ring (5 mm of diameter) was used to avoid air leaking from the mini permeameter nozzle. These authors reported meaningful variability of permeability and porosity between host rock and the different zones within the DBs (Fig. 3). Tondi *et al.* (2016) pointed out that the permeability between FIG and OFG differs in the range of two-to-three orders of magnitude despite their similar porosity. Zambrano *et al.* (2017) inferred that the permeability differences

186 between the grainstones pertaining to the distinct locations may be related to significant differences
 187 of connected porosity, specific surface area and connectivity.



190 Figure 3. Scatterplot of porosity and permeability of the studied carbonate grainstones. Data of porosity for the SVG
 191 (triangles) from Tondi *et al.* (2007), for FIG (circles) from Tondi *et al.* (2012), and for OFG (squares) from Tondi *et al.*
 192 (2016). Data of permeability for the SVG Antonellini *et al.* (2014), and for both FIG and OFG from Tondi *et al.* (2016).
 193 Error bars correspond to the standard error of the mean. Both axes are in logarithmic scale. Meaning of acronyms are HR:
 194 host rock, ZI: zone I, ZII: zone II, ZIII: zone III.

196 For the SR micro-CT experiments, five parallelepiped-shaped samples (with size of ~ 4 mm
 197 x 4 mm x 30 mm) were selected from the studied SVG, FIG and OFG rocks (Fig. 4). From the SVG,
 198 the studied sample (SVG-S1) contains a compactive shear band composed of three different zones (I,
 199 II, III; *sensu* Tondi *et al.* 2006) surrounded by undeformed host rock. From the FIG two samples were
 200 collected; one of the host rock (FIG-S2) and one belonging to a fault core of about 5 centimeters in
 201 thickness (FIG-S3). From the OFG two samples were selected; one composed entirely of host rock
 202 (OFG-S4) and the other includes a single DB (OFG-S5).

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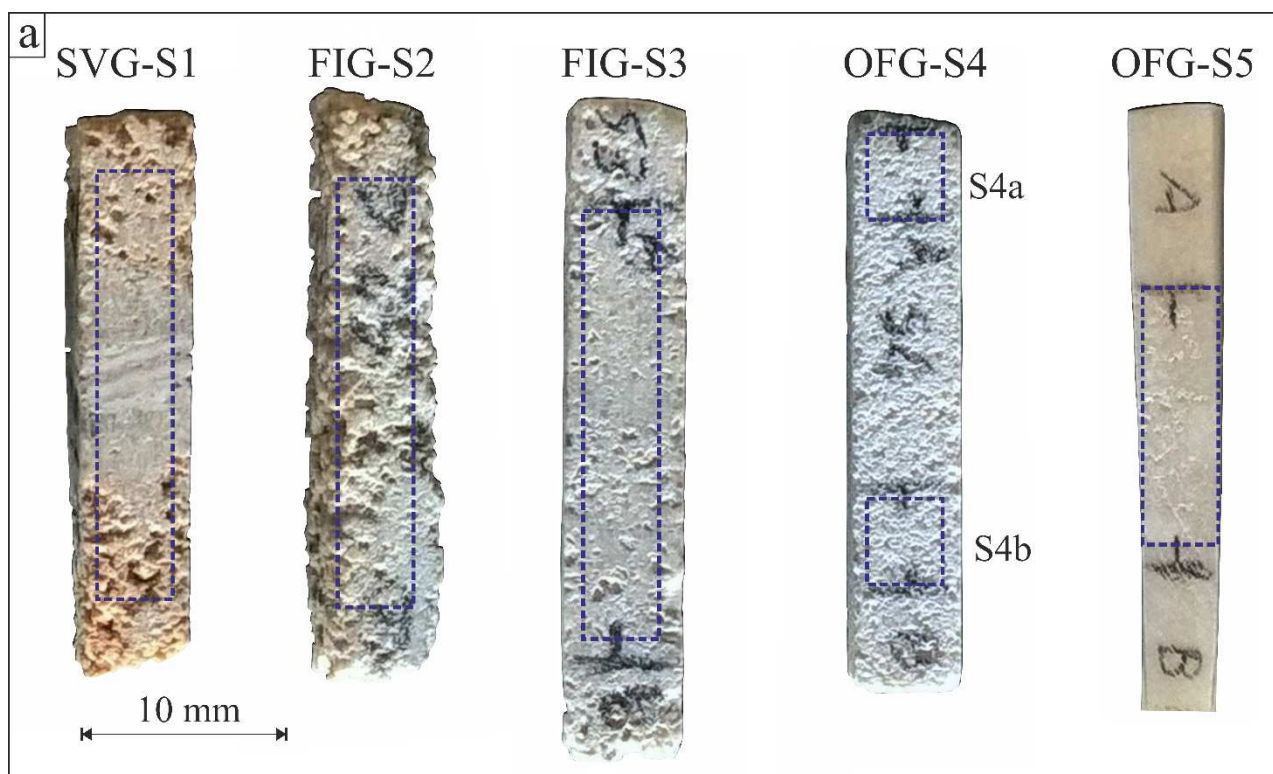


Figure 4. – Studied samples pertaining to deformed carbonate grainstones were obtained from outcrops located at northwestern Sicily (S1-S3) and Abruzzo (S4, S5) regions, Italy. a) Photograph of the original samples, the dotted areas correspond roughly to the imaged and analyzed volumes after removing the irregular edges. The longest axis of the samples is subparallel to bedding and orthogonal to the fault/DB zones (dipping 50°-90°, Tondi *et al.*, 2016).

2.2. Synchrotron radiation microtomography experiments

The SR micro-CT experiments and the image processing and analysis were performed following the methodology described by Arzilli *et al.* (2015) and Zambrano *et al.* (2017). The selected rock samples were imaged at the SYRMEP beamline of the Elettra laboratory. The X-ray beam delivered from a bending magnet source has a nearly-parallel geometry and a high spatial coherence (Abrami *et al.*, 2005; Tromba *et al.*, 2010) allowing to take advantage of phase contrast effects (Cloetens *et al.*, 1996). This beamline is suitable for obtaining 3D images of carbonate rocks and extracting valuable information about pores morphology, connectivity, and permeability at the pore scale (e.g. Gharbi and Blunt, 2012; Blunt *et al.*, 2013; Bijeljic *et al.*, 2013; Cilona *et al.*, 2014; Arzilli *et al.*, 2015; Zambrano *et al.*, 2017).

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663 220 Zambrano *et al.* (2017) obtained images at medium spatial resolution (voxel size = 9.0 μm)
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665 221 and high spatial resolution (voxel size = 2.4 μm) using the monochromatic and the white beam
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668 222 configuration of the beamline, respectively.

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670 223 For the images acquired in the monochromatic beam configuration, the sample-to-detector
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672 224 distance was set to 180 mm (propagation-based phase-contrast mode) and an X-ray energy of 34 keV
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674 225 was selected by a double-crystal Si monochromator. Each sample was placed on a high-resolution
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676 226 rotation stage, and a series of 1800 radiographs (projections) were acquired over a total angular range
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678 227 of 180° with an exposure time/projection of 3.5 sec. Projections were acquired by using a water-
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680 228 cooled, 12-bit, 4008 x 2672 pixels CCD camera (VHR, Photonic Science) with an effective pixel size
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682 229 of 4.5 μm . The camera chip was coupled to a Gadox scintillator screen through a fiber optics taper in
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685 230 order to convert the X-ray into visible light. Applying a 2x2 binning to the detector pixels, an output
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687 231 pixel size of 9.0 μm x 9.0 μm was used for image acquisition.

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689 232 A white beam configuration mode was used to image samples belonging to DBs or fault rock
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691 233 (Baker *et al.*, 2012) at higher spatial resolution, filtering the X-ray beam with 1.5 mm Si + 0.025 mm
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693 234 of Mo. The sample-to-detector distance was set at 150 mm. For each sample, 1800 projections were
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695 235 acquired over a total scan angle of 180° with an exposure time/projection of 2 s. The detector
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697 236 consisted of a 16 bit, air-cooled, sCMOS camera (Hamamatsu C11440-22C) with a 2048 \times 2048 pixel
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699 237 chip. The effective pixel size of the detector was set at 2.4 μm \times 2.4 μm , yielding a maximum field
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702 238 of view of about 5.0 mm \times 5.0 mm.

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704 239 The tomographic slice reconstruction was performed using the SYRMEP Tomo Project software
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706 240 developed at Elettra (Brun *et al.*, 2015) and powered by the ASTRA tomography toolbox (Palenstijn
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708 241 *et al.*, 2011) and TomoPy (Gürsoy *et al.* 2014). To improve the reliability of quantitative
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710 242 morphological analysis and enhance the contrast between solid and porous phase, a single-distance
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712 243 phase-retrieval algorithm was applied to the white beam projections (Fig. 4) using the Paganin's
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714 244 algorithm (Paganin *et al.*, 2002) based on the Transport of Intensity Equation (TIE).
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In the present work, the medium spatial resolution images were selected for the computational simulation. The criteria of this decision were made mainly based on the computational limitations, even though it may imply to do not take into account micro-pores in the simulations. Suitable volumes of interests (VOIs) were selected to assess the pore-network properties and estimate the permeability in host rock and DBs. The size of VOIs (see Table 1) was determined by the dimension of each evaluated region (i.e. host rock, ZI, II and III) within the sample. The whole imaged sample was included in the study in order to increase the representativeness of the results. In wide zones, such as the host rock, a high number of VOIs were evaluated, whereas, in thin zones, such as DBs, fewer VOIs with similar dimension were extracted.

The investigated VOIs images have a multiphase composition due to the content of voids, calcite grains, calcite cement, and silica grains (Zambrano *et al.*, 2017). For that reason, a 3D image segmentation was performed by the automatic multiphase k-means clustering algorithm (Hartigan, 1975; Hartigan and Wong, 1979), setting 3 to 4 classes of objects, depending on the sample. The segmentation was performed by using the *Pore3D* software library developed at Elettra (Brun *et al.*, 2010; Zandomenighi *et al.*, 2010). Then, a 3D bilateral filter (Tomasi and Manduchi, 1998) was applied to the reconstructed data for smoothing the images and preserving edges. Results are binary images composed of voids and grains. After this, the tool ‘Find Connected Structures’ of the Fiji software (Schindelin *et al.*, 2012) was used for dividing the pore space into two components: i) connected pores and ii) isolated pores. For the simulations, only the connected pore networks were used for easing the computation.

Table 1. VOIs dimensions and description

Sample	VOIs	Vol. [mm ³]	Volume [Voxels]	Description
SVG-S1	1HR	23.33	400 x 400 x 200	Host rock
	2HR	23.33	400 x 400 x 200	Host rock
	3HR	23.33	400 x 400 x 200	Host rock
	4ZIII	27.99	400 x 400 x 240	Zone III, highly cemented
	5FC	34.99	400 x 400 x 300	Fault core, with a slip surface
	6ZIII	17.50	400 x 400 x 150	Zone III, highly cemented
	7HR	23.33	400 x 400 x 200	Host rock
	8HR	23.33	400 x 400 x 200	Host rock
FIG-S2	1HR	43.74	500 x 400 x 300	Host rock
	2HR	43.74	500 x 400 x 300	Host rock
	3HR	43.74	500 x 400 x 300	Host rock
	4HR	43.74	500 x 400 x 300	Host rock
	5HR	43.74	500 x 400 x 300	Host rock
	1CEM	39.37	400 x 450 x 300	Fault core, highly cemented
	2CEM	39.37	400 x 450 x 300	Fault core, highly cemented
FIG-S3	3MIX	39.37	400 x 450 x 300	Fault core, partially cemented
	4MIX	39.37	400 x 450 x 300	Fault core, partially cemented
	5CEM	39.37	400 x 450 x 300	Fault core, highly cemented
	6CEM	39.37	400 x 450 x 300	Fault core, highly cemented
	7MIX	39.37	400 x 450 x 300	Fault core, partially cemented
	8DISS	39.37	400 x 450 x 300	Fault core, affected by dissolution
OFG-S4	1HR	44.29	450 x 450 x 300	Host rock
	2HR	44.29	450 x 450 x 300	Host rock
OFG-S5	1HR	34.99	400 x 400 x 300	Host rock
	2MIX	34.99	400 x 400 x 300	Partially cemented zone
	3CEM	34.99	400 x 400 x 300	Highly cemented zone
	4MIX	34.99	400 x 400 x 300	Partially cemented zone
	5MIX	34.99	400 x 400 x 300	Partially cemented zone

2.3. Lattice-Boltzmann method and permeability calculation

Lattice-Boltzmann simulations were performed by means of the open-source computational fluid dynamics software PALABOS (Latt, 2009) using a modified version of the methodology previously described by Degruyter *et al.*, (2010). The methodology consists in imposing a simple-phase fluid flow through the segmented 3D images by maintaining a fixed pressure gradient between the inlet and outlet faces of the volume, the rest of the faces were padded. The interface pores-voids was converted to bounce-back boundary conditions. The main difference with the methodology proposed by Degruyter *et al.* (2010) is the replacement of the collisional operator BGK by an MRT (d'Humières *et al.*, 2002) with a D3Q19 lattice.

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843 277 The simulation ended once the imposed steady state condition was reached (standard
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845 278 deviation of the average energy $<10^{-4}$ after 1000 steps, Degruyter *et al.*, 2010). After that, the
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847 permeability component parallel to the imposed flow was calculated applying the Darcy's law,
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$$849 \frac{\delta P}{\delta x} = \frac{\mu}{k} U, \quad (\text{equation 2})$$

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853 281 where, $\delta P/\delta x$ is the pressure gradient, μ the fluid kinematic viscosity, and U the average fluid
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855 282 velocity per unit of area. The permeability was calculated, using the same procedure, in three
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857 283 orthogonal directions two parallel to the DBs (k_x and k_y) and the third one perpendicular to the DB
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859 284 (k_z). All the variables are handled in lattice units before the permeability calculation, results are
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861 285 transformed to real world units multiplying by the effective length of the voxel side in meters. To
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863 286 guarantee a flow in the laminar regime, and therefore the validity of Darcy's law, it was evaluated
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865 287 that the permeability keeps stable among different pressure gradients (Degruyter *et al.*, 2010). The
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867 288 obtained permeability values are not considered as absolute due to the possible source of error caused
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869 289 by the resolution of the micro-CT images and the few number of samples evaluated during the
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871 290 experiments.
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874 291 2.4. Analysis of the effective pore-network properties

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879 293 After the simulations, the resulting lattice velocity volumes were segmented with a single
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881 294 threshold (lattice velocity >0) for obtaining the effective pore space contributing to the flow. The 3D
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883 295 visualization of the output images was obtained by the volume rendering procedure, using the
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885 296 commercial software VGStudio MAX 2.0 (Volume Graphics) and the software Paraview (Ahrens *et*
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887 297 *al.* 2005). The assessment of the segmented pore space was made using the *Pore3D* software library,
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889 298 which has been optimized for quantitative examination of X-ray micro-CT images of porous media
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891 299 and multiphase systems and includes several modules, such as filtering, morphological, anisotropy
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893 300 and skeleton analysis. The analyzed properties were the effective porosity, the specific surface area,
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895 301 and the tortuosity in three directions (x , y , z) corresponding to the fluid flow experiments.
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903 302 The effective porosity (Φ) here is defined as the ratio of the pore volume with a non-zero
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905 303 velocity and the total volume of the sample. The specific surface area (S) is defined as the ratio of the
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908 304 surface in contact with fluid and the total volume. The tortuosity (τ) has a vast number of definitions
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910 305 based on geometrical, hydraulic, electrical, and diffusion parameters (Ghanbarian *et al.*, 2012 and
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912 306 references therein). In this work, the method used to evaluate the tortuosity is based on the direct
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914 307 measurement of the shortest distance between two points in the pores (Gommes *et al.*, 2009). The
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916 308 geometrical tortuosity is calculated as $\tau = L_g/L_e$, where L_g is the geodesic length defined as the
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918 309 shortest path connecting two points in the pore space, and L_e is the Euclidean length (Soille, 1999;
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920 310 Dunsmuir *et al.*, 1991).

922 311 923 924 925 312 **2.5. Representativeness evaluation of results**

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928 313 The representative elementary volume (REV) is defined as the volume in which the variability
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930 314 of a property (e.g., porosity, specific surface area, tortuosity, permeability) tends to decay
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932 315 significantly, enclosing a representative amount of the sample heterogeneity (Bear, 1972;
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934 316 Zandomeneghi *et al.*, 2010). The REV must be sufficiently larger to include a considerable number
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936 317 of pores to permit the meaningful statistical average required in the continuum concept (Bear, 1972).
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938 318 Several authors have studied the existence and the dimensions of a REV for different porous materials
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940 319 (Zhang *et al.* 2000; Al-Raoush and Papadopoulos 2010; Mostaghimi *et al.* 2013). Zhang *et al.* (2000)
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942 320 introduced the term of a 'statistical REV' for heterogeneous media, which is defined as the volume
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945 321 beyond which the mean becomes approximately constant and the coefficient of variation (C_v , defined
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947 322 as the ratio of the arithmetic mean divided by the sample standard deviation) is lower than a threshold
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949 323 value (e.g. $C_v < 0.2$). Al-Raoush and Papadopoulos (2010) proposed that the determination of the
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951 324 REV should be determined using the porosity distribution over different volumes. Mostaghimi *et al.*
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953 325 (2013) investigated the existence and size of REV for samples of sandstones and carbonate rocks
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955 326 using permeability, specific surface area, and porosity. These authors estimated that the necessary

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327 size of REV for the permeability evaluation should be larger than that for porosity and specific surface
328 area. In this work, the statistical REV approach proposed by Zhang *et al.* (2000) is used.

2.6. Single cylindrical-shape pore experiments

331 In order to quantify the effect of resolution on the evaluated properties, a cylindrical-shape
332 fictitious pore of radius, r , was considered. Downscaling the resolution, the porosity, specific surface
333 area and permeability were calculated from the images and compared with the analytical values. The
334 permeability is analytically derived from combining the Poiseuille's Equation for flow through a
335 cylinder pipe with the Darcy's Law for flow in porous media,

$$k = \frac{\pi r^2}{8} \quad (\text{equation 3})$$

337 The results are normalized by the analytical values and plotted against the pore radius expressed
338 in terms of number of voxels. In this way the observations could be applicable to any pore radius.

3. Results

The results of the MRT-LBM simulations are the calculated permeability and the lattice velocity volumes (Fig. 5- 7). From the lattice velocity volumes additional properties were quantitatively analyzed including the effective porosity, specific surface area and tortuosity of the pore network contributing to the permeability of the host rock and DBs. The multidirectional (axes x, y, and z) results of both quantitative pore network analysis and permeability calculated with LBM simulation are summarized in Table 2. As it was stated in the methods section, for each zone (i.e. HR, ZI, ZII, ZIII) the average values corresponded to the arithmetic mean, in the case of k_z and k_y , or the harmonic mean, in the case of k_x . In specific cases, only one measurement was obtained due to the dimension of the analyzed zone. The results of the effective porosity, specific surface area, and tortuosity were plotted with the corresponding value of calculated (LBM) permeability (Fig. 8) with the intention of evaluating their respectively control on permeability. Data is divided in pristine rocks and fault zones to individuate the effect of deformation and diagenesis on the pore network and permeability within DBs. The combined control of these properties was evaluated considering the Kozeny-Carman equation (Fig. 8d), however the intention was not to test the accuracy of this equation.

3.1. MRT-LBM simulations

In the case of host rocks, the SVG (Fig 5b, d) and FIG (Fig. 6d) showed a combination of both wide and narrow conduits. In both velocity volumes, it is shown how the wider diameter of conduits allows the fluid to reach higher velocities in comparison to the narrow conduits. Differently, in the host rock pertaining to the OFG the pore-network is represented by a high number of very thin fluid conduits (Fig. 7c, e). The dimension of the pore diameter seems to be related to the specific surface area (Table 2), where the lower values correspond to the FIG and the higher values to OFG host rocks.

For sample SVG-S1, velocity volumes indicated that the fluid conduits within the DB are significantly fewer than those of the host rock. Within the cemented zone, ZIII, the fluid flow

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1083 366 experiments failed due to the absence of a connected pore-network. Within the fault core (Fig. 5c),
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1085 367 the fluid flow is negligible in a direction perpendicular to the DB. However, the fluid flow is present
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1087 368 through the space generated by the distribution of asperities within the slip surfaces. This pore-
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1089 369 network is characterized by wide and anastomose conduits that concentrated the fluid flow through
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1091 370 the sharp discontinuity. Solution-enlarged stylolites may also represent secondary pathways for flow.
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1093 371 The obtained permeability shows significant differences between the HR and the different
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1095 372 zones composing the DB (Zones III, II, I). The HR exhibited high and isotropic values of permeability.
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1097 373 In the cemented zones, the permeability is negligible in all directions (e.g. SVG-S1, OFG-S5) due to
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1099 374 the absence of connected pores (Fig. 10). Within the fault cores, the permeability decreases by nearly
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1101 375 two orders of magnitude and sometimes presents important anisotropy. In the case of the fault core
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1103 376 of SVG-S1 (composed by ZIII and I), the permeability component perpendicular to the DB is zero,
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1105 377 whereas the permeability components parallel to the DB are possible thanks to the presence of
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1107 378 channelized pore-network. In the case of FIG-S3, the fault core is characterized by alternation of
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1109 379 zones affected by cementation and dissolution creating a highly heterogeneity and anisotropy. In the
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1111 380 studied samples, the permeability component perpendicular to the DB is null for the fault cores.
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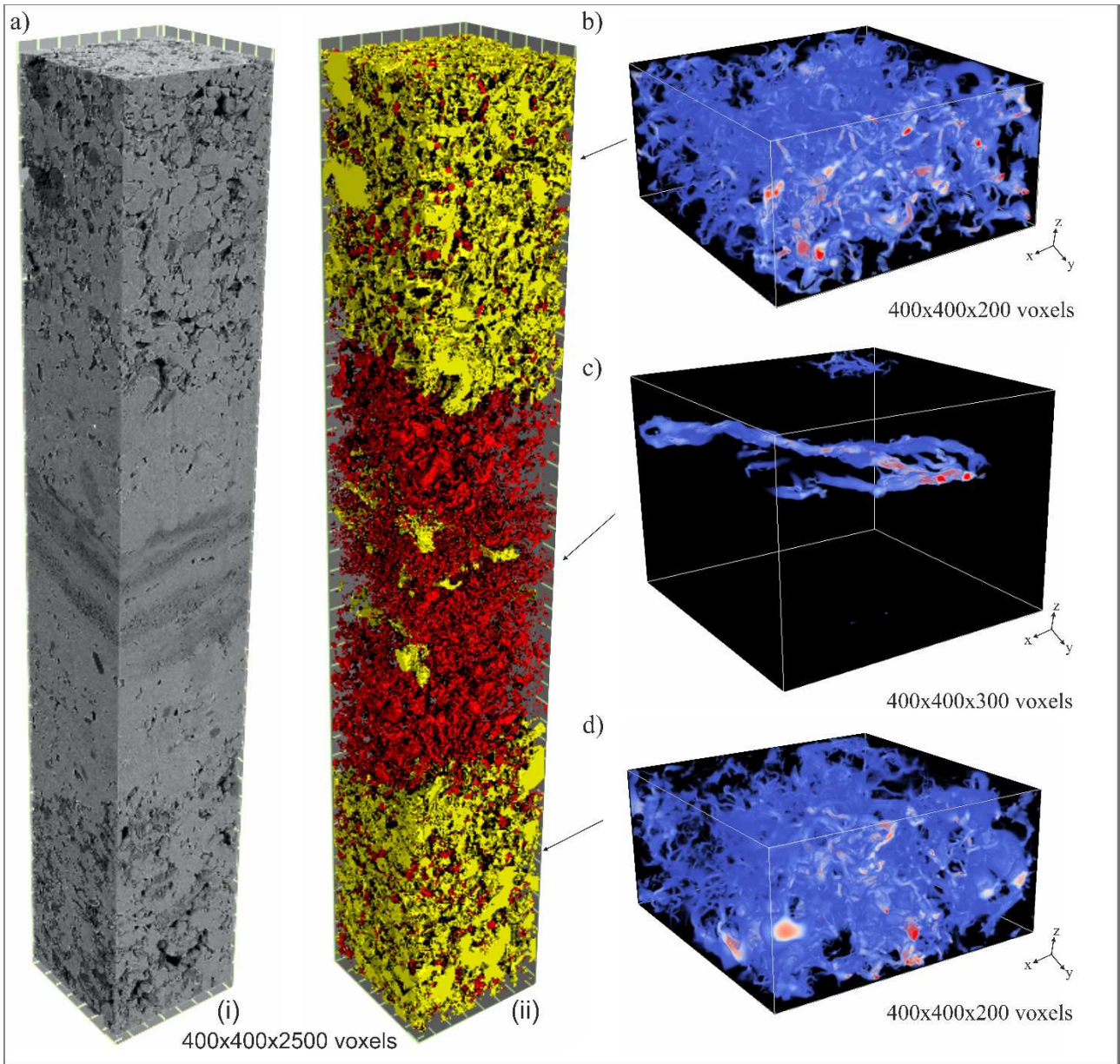


Figure 5.- a) Sample SVG-S1 with the volume rendering of the (i) raw reconstructed SR micro-CT images (voxel size = 9 μm) and (ii) segmented pores space (connected pores in yellow and unconnected pores in red, after Zambrano *et al.* 2017). Detail of lattice velocity volumes from the b) and d) host rock, and c) fault core. In the fluid velocity volumes, high velocities in lattice units are represented by warm colors. The z-axis of the volumes is perpendicular to the DB.

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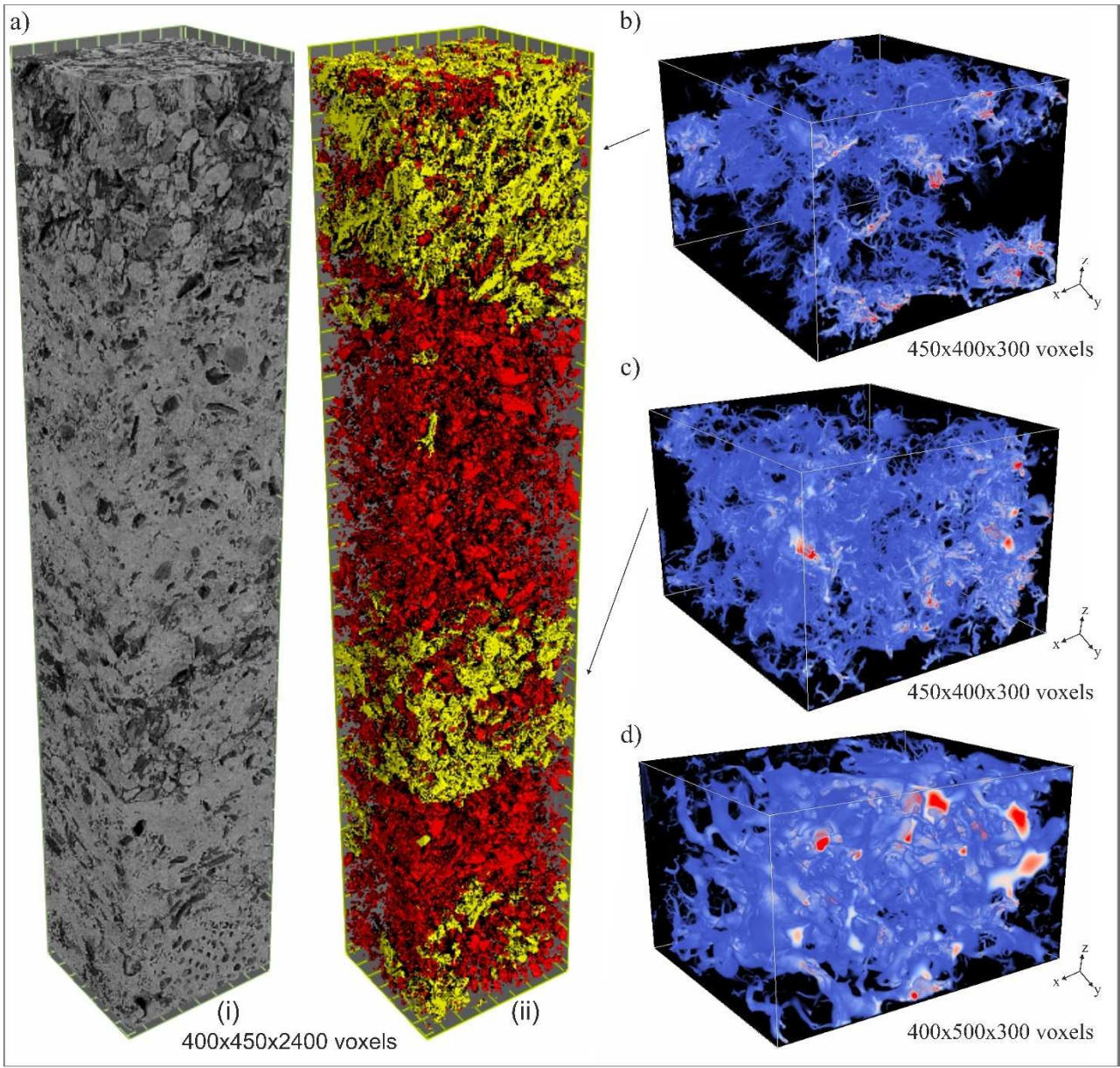


Figure 6.- a) Sample FIG-S3 with the rendering of the (i) raw reconstructed SR micro-CT images (voxel size = 9 μm) and (ii) segmented pores space (connected pores in yellow and unconnected pores in red, after Zambrano *et al.* 2017). Detail of lattice velocity volumes from the b) and c) fault core, and d) host rock from the sample FIG-S2. In the fluid velocity volumes, high velocities in lattice units are represented by warm colors. The z-axis of the volumes is perpendicular to the DB orientation.

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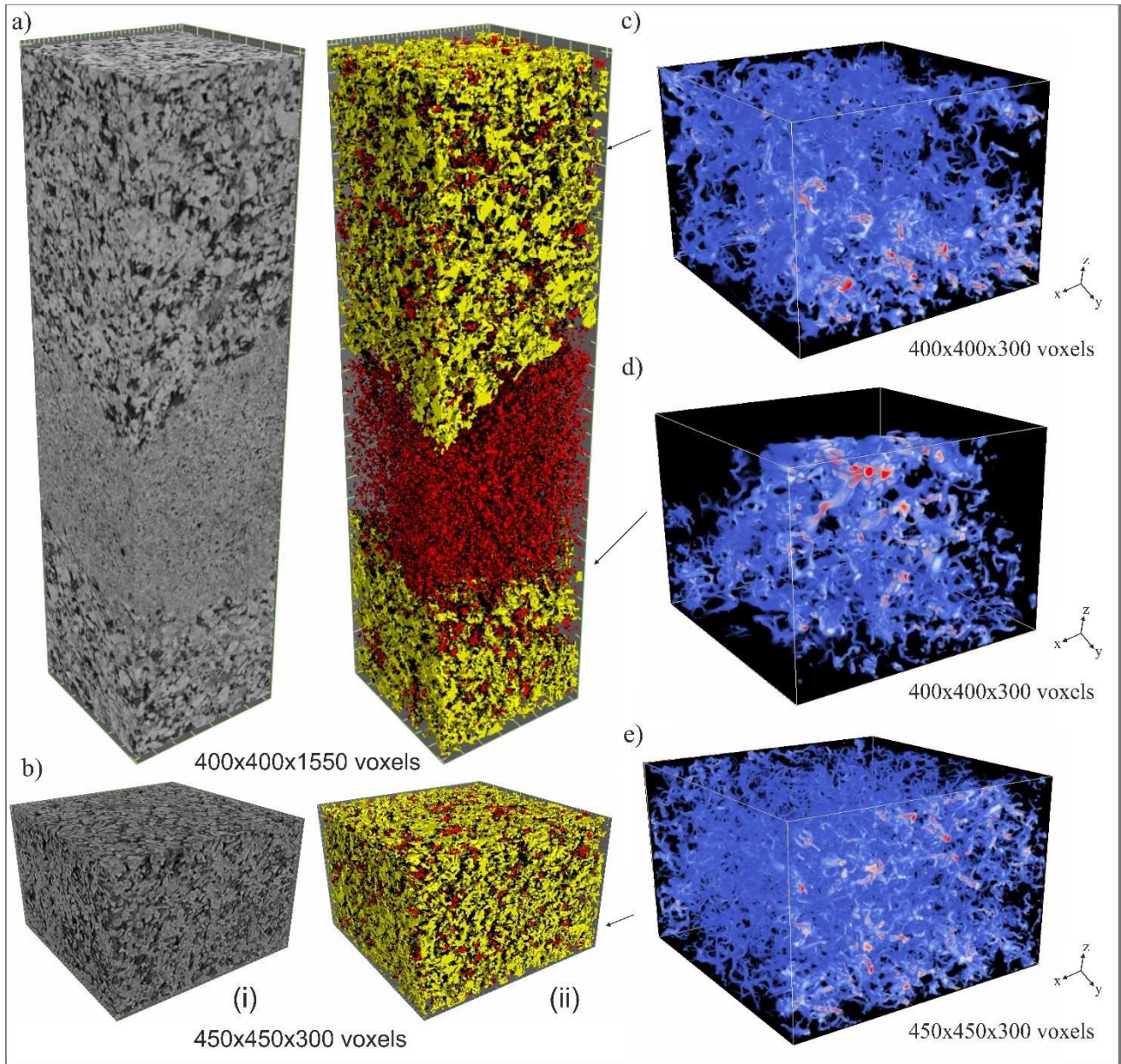


Figure 7.- a) Sample OFG-S5 (DB) and b) OFG-S4a (host rock) with the rendering of the (i) raw reconstructed SR micro-CT images (voxel size = 9 μm), and (ii) segmented pores space (connected pores in yellow and unconnected pores in red, after Zambrano *et al.* 2017). Detail of lattice velocity volumes from the c) host rock (near to the DB), e) host rock (far from DB), and d) transition between DB and host rock. In the fluid velocity volumes, high velocities in lattice units are represented by warm colors. The z-axis of the volumes is perpendicular to the DB orientation.

Table 2. Results of the quantitative pore network analysis and permeability calculation with

LBM.

Sample	Zones		Φ_x [%]	Φ_y [%]	Φ_z [%]	S_x [mm ²]	S_y [mm ²]	S_z [mm ²]	τ_x [-]	τ_y [-]	τ_z [-]	k_x [m ²]	k_y [m ²]	k_z [m ²]
SVG-S1	Host Rock	Mean	12.87	14.13	12.07	45.9	47.0	42.5	2.9	2.7	3.7	9.5x10 ⁻¹³	2.4x10 ⁻¹²	2.3x10 ⁻¹²
		SE	0.69	0.28	0.52	4.6	5.7	3.4	0.4	0.1	0.4	3.1x10 ⁻¹³	8.7x10 ⁻¹³	2.6x10 ⁻¹²
		Cv	0.09	0.03	0.07	0.17	0.21	0.14	0.30	0.06	0.25	0.57	0.64	1.06
	Zone III	Value	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	0.0	0.0	0.0
	Fault Core	Value	2.00	2.00	0.0	39.6	40.3	0.0	3.1	2.9	-	3.0x10 ⁻¹³	3.2x10 ⁻¹³	0.0
FIG-S2	Host Rock	Mean	26.15	26.55	28.10	28.8	28.6	29.6	1.6	1.9	1.9	2.9x10 ⁻¹¹	6.0x10 ⁻¹¹	3.1x10 ⁻¹¹
		SE	1.15	1.55	1.60	0.6	1.1	1.1	0.2	0.3	0.2	1.3x10 ⁻¹¹	3.7x10 ⁻¹¹	2.0x10 ⁻¹¹
		Cv	0.06	0.08	0.08	0.03	0.06	0.05	0.20	0.33	0.20	0.77	1.08	0.68
FIG-S3	Fault Core	Mean	5.19	5.36	2.11	35.1	35.4	7.2	3.1	3.8	2.2	3.3 x10 ⁻¹³	2.1 x10 ⁻¹³	0.0
		SE	2.13	2.13	2.11	14.5	14.7	7.2	0.1	0.2	1.6	1.0 x10 ⁻¹³	3.7x10 ⁻¹⁴	0.0
		Cv	1.09	1.07	2.65	1.02	1.02	2.65	0.10	0.12	1.03	0.81	0.46	2.8
OFG-S4	Host Rock	Mean	12.48	12.73	11.90	78.2	77.2	77.6	3.2	3.2	4.0	4.0x10 ⁻¹³	3.6x10 ⁻¹³	4.2x10 ⁻¹³
		SE	0.91	0.97	0.53	1.7	2.0	1.7	0.1	0.2	0.2	1.5x10 ⁻¹³	6.8x10 ⁻¹⁴	1.7x10 ⁻¹³
		Cv	0.145	0.13	0.09	0.043	0.045	0.044	0.045	0.15	0.11	0.73	0.33	0.52
OFG-S5	DB-	Mean	6.32	6.16	6.58	57.5	58.0	55.8	3.8	3.5	3.7	2.6x10 ⁻¹³	7.4x10 ⁻¹³	2.1x10 ⁻¹³
		SE	1.88	1.84	1.38	0.9	1.0	2.5	0.3	0.3	0.3	1.2x10 ⁻¹³	2.6x10 ⁻¹³	9.2x10 ⁻¹⁴
		Cv	0.67	0.67	0.47	0.033	0.034	0.10	0.16	0.20	0.17	1.01	0.79	0.60

3.2. Pore-network properties

All the evaluated host rocks showed a high effective porosity. The greatest effective porosity values in the host rock correspond to the FIG with a mean of 26.93 ± 0.75 %, followed by the SVG with a mean porosity of 13.02 ± 0.4 %, whereas the host rock of FIG showed a mean effective porosity of 12.33 ± 0.43 %. Within the DB hosted in SVG, the zones with high cementation, ZIII, are likely to have zero effective porosity, whereas, in the fault core with pore network composed of enlarge stylolites and slip surfaces, ZII and ZI respectively, the effective porosity is relative higher (about 2.0%). In the case of the fault core of FIG-S3, there is a high variability of effective porosity ($C_v > 1.0$) due to the alternation of volumes affected by cementation or dissolution. VOIs is highly affected by cementation showed null porosity values, whereas in VOIs highly affected by dissolution the porosity could reach 15.1 %. Volumes partially cemented indicated a null porosity in the z-direction (perpendicular to the fault), whereas is about 7.26 ± 0.29 % for the other directions. Considering all the VOIs, the mean porosity tensor for the fault core sample FIG-S3 is Φ (5.19 ± 2.13 %; 5.36 ± 2.33

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1384 420 %; 2.11 ± 2.11 %). In the case of OFG-S5, some spot (with dimension lower than the VOIs) where
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1386 421 well-cemented and presented null porosity. The mean porosity tensor for the OFG-S5 is Φ ($1.88 \pm$
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1388 422 0.67 %; 1.84 ± 0.67 %; 1.38 ± 0.47 %). The coefficient of variation (Cv) showed values up to 0.67
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1390 423 for the porosity of this sample, which indicates an important heterogeneity. The scatter plot porosity-
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1392 424 permeability (Fig. 8a) indicates an important control of the porosity on permeability and a clear
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1394 425 differentiation between undeformed host rock and deformed/cemented zones.

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1396 426 The specific surface area indicates higher values for the host rock pertaining to OFG (77.71
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1398 427 ± 0.28 mm⁻¹) in comparison to the host rocks of SVG (45.15 ± 0.80 mm⁻¹) and FIG (29.03 ± 0.19 mm⁻¹).
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1400 428 In the case of DBs, the specific surface area could increase within the host rock in zones affected
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1402 429 by dissolution and cataclasis as in FIG-S3 (about 60.0 mm⁻¹). Also, this could decrease is the
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1404 430 dominant process is the cementation as in OFG-S5 (57.01 ± 0.28 mm⁻¹) or, in the extreme case, SVG-
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1406 431 S1-ZIII characterized by high cementation and null effective porosity. As it was expected, the specific
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1408 432 surface area seems to be inversely related to the permeability (Fig. 8b). However, there is not a clear
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1410 433 differentiation of deformed and pristine rock possible related to the effect of deformation and
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1412 434 diagenetic processes involved.

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1414 435 Concerning the geometrical tortuosity (Table 2), the values in the host rocks are 1.79 ± 0.04
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1416 436 for FIG, 3.07 ± 0.05 for SVG, and 3.46 ± 0.04 for OFG-S4. In the case of DBs, the geometric
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1418 437 tortuosity could increase in the case of FIG-S3 (3.22 ± 0.08) and OFG-S5 (3.67 ± 0.04). The tortuosity
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1420 438 seems to be inversely related to the permeability (Fig. 8c).

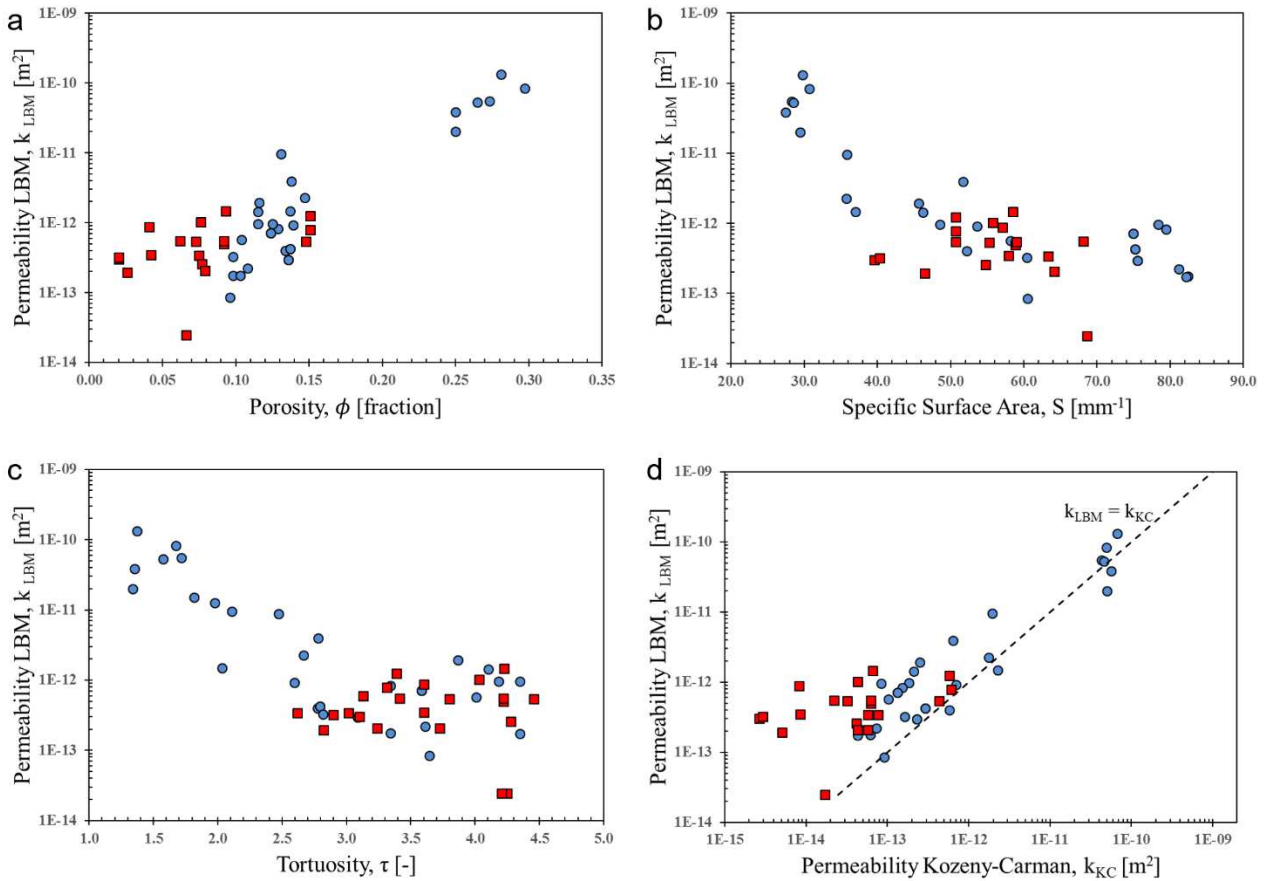


Figure 8. - Relationship between LBM permeability and a) effective porosity b) specific surface area c) geometrical tortuosity, and d) permeability estimated with the K-C equation. Host rock data is represented by blue circles, whereas deformed rock data is in red squares. In (d) the dotted line represents the equality between calculated (LBM) and estimated (K-C) permeability. The axis containing permeability data are in logarithmic scale.

3.3. Single cylindrical-shape pore experiments

The effect of resolution on the evaluated properties was assessed considering a single fictitious cylindrical-shape pore. Both porosity and specific surface are related to the resolution by a non-linear function (Figs. 9). For a pore with diameter represented by 10 voxels, both properties are less than 20% lower than the theoretical value. The permeability does not show significant variation (<10%) until the diameter of the pore is about 10 voxels (Fig. 9).

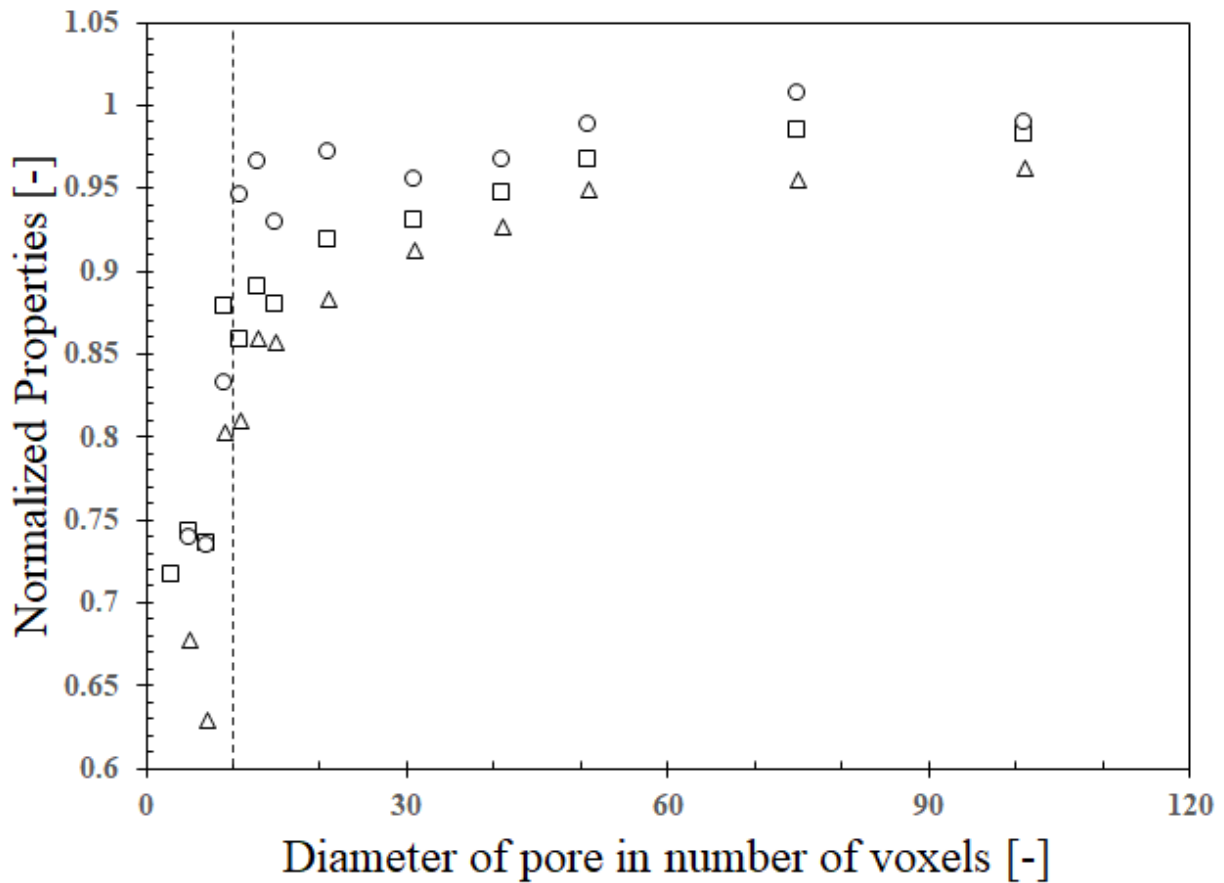


Figure 9. – Effect of image resolution (diameter of pore in number of voxel) on the evaluated pore properties: porosity (squares), specific surface area (triangles), and LBM permeability (circles). The properties are normalized by the corresponding analytical values. The vertical dotted line indicates a threshold value of the resolution below which the difference of the measured permeability with the analytical value is higher than 10%.

4. Discussion

4.1. Permeability variability

Within the studied DBs different processes could take place such as cementation, pressure solution, cataclasis, and shearing along sharp discontinuities. The DB hosted in SVG presents well-differentiated tabular zones where pore-network varies due to different processes. The cementation process generally occurs in the outer zone of the band, ZIII, characterized by the precipitation of cement and absence of pore-throat collapsing (Tondi, 2007). According to the observations, the permeability is negligible due to the isolation caused by the cementation. The only porosity in this

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1564 466 zone reported by Zambrano *et al.* (2017) corresponds to isolated pores such as chambers within the
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1566 467 bioclast, which do not contribute to the fluid flow. In the case of ZII, the compaction may cause the
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1568 468 reduction of the primary pore-connectivity by collapsing the pore-throats. However, the same process
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1570 469 also generates stylolites by pressure solution at the grain-to-grain contact (Tondi, 2007). It was
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1572 470 observed that these stylolites, possible enlarged by dissolution, create thin pore conduits preferably
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1574 471 connected to the DB. Due to the cataclastic nature of ZI, connected pores, if are present, may be
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1576 472 below the resolution of the images and therefore not detected. However, if this is the case, the
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1578 473 contribution to the permeability should of minor importance. Within the ZI, the fluid flow is possible
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1580 474 through the space generated by the distribution of asperities within the slip surfaces. This pore
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1582 475 network is characterized by wide and anastomose conduits that concentrate the fluid flow through the
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1584 476 sharp discontinuity. The contribution to the permeability of the sharp discontinuity is very important
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1586 477 in parallel direction of the DB. In fact, the total permeability of the FC reaches values just one order
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1588 478 of magnitude less than the porous host rock in that direction. The permeability in an orthogonal
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1590 479 direction to the DB is negligible due to the presence of ZI and ZII. Basically, the hydraulic behavior
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1592 480 of the DB could be considered as a fracture surrounded by tight walls. This characteristic may have
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1594 481 some implications to the modeling of those structures during the reservoir characterization.
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1598 482 In the case of the fault core sample of FIG (FIG-S3), there are not differentiated zones like in
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1600 483 the DB form SVG. However, in this fault core there is an alternation of zones affected by cementation
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1602 484 and dissolution, which are oriented subparallel to the main fault direction. The variability is well
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1604 485 represented by great values of coefficient of variation especially in the z-direction ($C_v=2.8$), which
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1606 486 indicates a high heterogeneity (Zhang *et al.*, 2000). This variability may be caused by localized
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1608 487 cementation, compaction, dissolution and cataclasis. Moreover, the sample presents a high
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1610 488 permeability anisotropy due to the fact that the fluid flow is only allowed subparallel to the fault and
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1612 489 inhibited in the perpendicular direction. Comparing to the host rock (FIG-S2), the permeability values
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1614 490 in the parallel direction are reduced by about two orders of magnitude.
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1624 491 In the samples from FIG, there is a slight variation of permeability in the deformed areas with
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1626 492 respect to the pristine rock. There is neither an important anisotropy in the permeability. However,
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1628 493 the values of the coefficient of variation are slightly higher in the FIG-S5 in comparison to FIG-S4
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1630 494 indicating a greater heterogeneity of the permeability. The interpretation of these results is that the
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1632 495 deformation band is incipient with a minor effect on the permeability distribution.
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1634 496 In the host rocks the permeability is mostly isotropic. Some minor differences among
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1636 497 permeability components related to changes in the texture of the pores and grain size composing the
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1638 498 rocks. Considering the open discussion made by Tondi (2016), we may confirm that the permeability
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1640 499 is controlled by the grains/pores size and the tortuosity of the
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1642 500 1643 1644 1645 501 4.2. Dependency of permeability on connected pore-network properties 1646

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1649 503 As it was expected, results indicated that the permeability seems proportional to the effective
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1651 504 porosity and inversely proportional to both the specific surface area and the tortuosity (Fig.8a-c). The
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1653 505 specific surface area has a very important effect on the permeability due to a greater surface in contact
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1655 506 with the fluid that causes more friction to fluid motion. The dependency of permeability on the
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1657 507 aforementioned pore-network properties has been previously stated by several authors (e.g. Kozeny,
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1659 508 1927; Carman, 1937; Archie, 1942; Wyllie and Rose, 1950; Swanson, 1981; and Katz and Thompson,
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1661 509 1986). In a closer case, the control exerted by these properties have been claimed by Tondi *et al.*
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1663 510 (2016) to explain permeability differences in three orders of magnitude between porous carbonate
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1665 511 grainstones pertaining to FIG and OFG.

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1668 513 Even though our intention was not to prove the validity of the Kozeny-Carman equation, the
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1670 514 estimated permeability with this method was plotted against the LBM permeability (Fig. 8d). In
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1672 515 general, the data shows an important scatter and seems not to fit properly to the equality line
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1674 516 ($k_{LBM}=k_{KC}$). It was noticed that this scatter seems to be higher in the VOIs pertaining to
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4.3. Validity and representativeness of results

The heterogeneity of the analyzed rocks has been described by the coefficient of variability (Cv). Zhang *et al.* (2000) indicated that a low Cv indicates that the results could be considered as representative statistically, which made it a good substitute of the well-known concept of REV. Considering the nature of the simulation experiments, the use of a statistical approach to find representative results is less straightforward and faster than to consider bigger volumes. The heterogeneity varies in function of the measured properties and the type of rock (i.e. HR and DB). In general, the permeability presents more variability with respect to the porosity, specific surface area and tortuosity. This stands to reason, because the permeability is depending of such properties (eq. 1). Mostaghimi *et al.* (2013) found comparable results, in which they concluded that the representativeness of a volume depends upon the evaluated property. As it was expected, the DB samples are more variable than the pristine rocks. This is related to the presence of bands or zones dominated by cementation, cataclasis or dissolution. The alternation of such bands may cause a high variability in all properties, especially in the permeability in the z-direction (perpendicular to the DB/fault plane). Considering these results, we consider that a larger number of samples are necessary to provide representative results for applications in reservoir simulation. However, for the scope of this work the variability was useful to characterize the heterogeneity and its implications at the pore scale.

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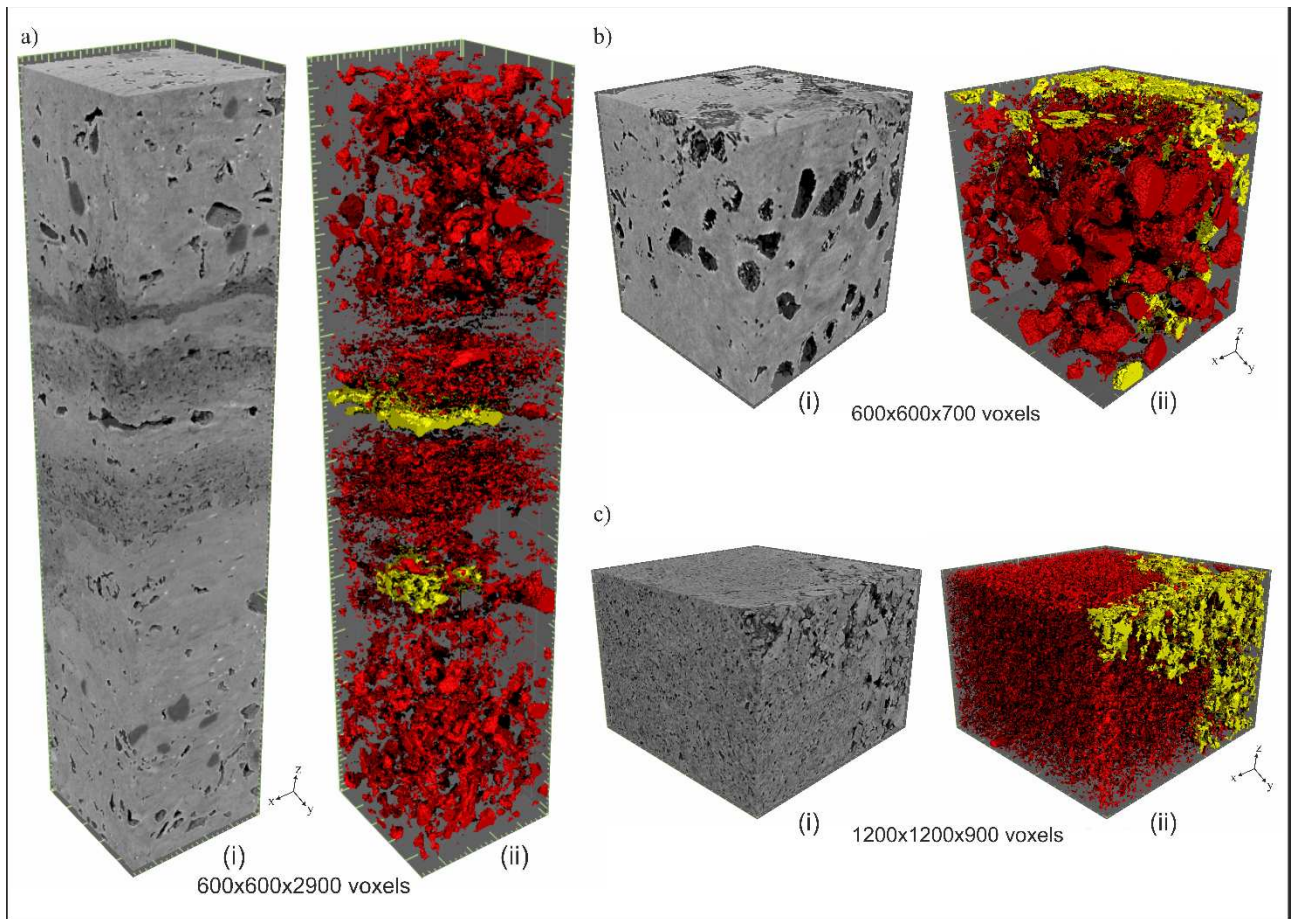


Figure 10.- DBs volumes at high resolution (voxel size = 2.4 μm) pertaining to a) Sample SVG-S1, b) Sample FIG-S3, and c) Sample OFG-S5. For each volume it is shown the (i) raw reconstructed SR micro-CT images and (ii) segmented pores space (connected pores in yellow and unconnected pores in red, after Zambrano et al. 2017). The z-axis of the volumes is perpendicular to the DB.

This study did not aim at providing exact values of permeability or to prove the accuracy of the LBM. However, permeability results are similar (one order of magnitude of difference) to the data obtained *in situ* by Antonellini *et al.* (2014) and Tondi *et al.* (2016) using an air permeameter. Nevertheless, it is necessary to take into consideration that these authors provided an important number of measurements and covered a total volume significantly greater than in the present work. On the other hand, the permeability obtained using an air permeameter may be also inaccurate. Filomena *et al.* (2014) reported that this technique applied to unconfined rock volumes (e.g. outcrop measurements) may be overestimated (about 37%) due to the shorter flow trajectories and a reduced rock volume in comparison with confined volume methods.

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1804 552 A key point for the validity of the results is the resolution of the images (voxel size = 9 μm)
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1807 554 connected pores were detected in the cemented zones within the DBs (Fig. 10). While, in both host
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1810 555 rocks and zones affected by dissolution pores the pores are significantly wide (more than 100 μm).
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1812 556 In agreement with Arzilli et al. (2015), studying similar grainstones of the Bolognano Fm., it is
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1814 557 assumed that the contribution of the micropores to the permeability may be negligible if compared to
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1816 558 the one of macropores. Nevertheless, the shape of imaged pores may be pixelated due to the resolution
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1818 559 of the images affecting the measured properties (i.e. porosity, specific surface area, and permeability).
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1820 560 In fact, these properties varied significantly in function of the resolution as it was found for a single
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1822 561 pore evaluation (Fig. 9). The permeability seems to be constant and close to the theoretical value until
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1824 562 certain threshold is reached (about 10 voxels of diameter). This result may be explained as a sort of
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1826 563 compensation of the contrary effect on permeability exerted by the porosity and the specific surface
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1828 564 area. Therefore, our results could infer that the presence of pores with a diameter lower than 100 μm
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1830 565 may cause an underestimation of the permeability. Based on these evidence, the measured properties,
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1832 566 including the permeability, may be slightly underestimated. However, the method used in this study
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1834 567 and the results obtained allowed us to obtain textural and petrophysical properties of realistic rocks
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1836 568 with a tensorial approach. In addition, it was put in evidence the control exerted by the textural
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5. Conclusions

The presented study used the lattice-Boltzmann method (LBM) for obtaining permeability values of deformed carbonate grainstones using segmented 3D images obtained by synchrotron X-ray microtomography. The experiments consisted of inducing pressure-driven flow through the virtual rock samples and deriving the permeability by means of the Darcy's law.

The permeability and effective porosity decrease within deformation bands (DBs) due to the combination of grain translation, rotation, compaction, cataclasis, and cementation processes. Pore-throats are collapsed and occluded by processes mentioned above. The remaining porosity does not contribute to fluid flow as it is mostly isolated. In the zone III, the cement could fully occlude the pore network resulting in a local barrier for fluid flow in the direction perpendicular to the DB/fault. In the zone II, the compaction likely causes intergranular pore collapsing but when pressure dissolution takes places the resulting stylolites may contribute to the fluid flow, especially in the directions subparallel to the DB/fault. Concerning the zone I, the grain size reduction contributes to the occlusion of the intergranular pores. These processes could lead to negligible permeability values within the cataclastic zone. However, if sharp discontinuities are present, the distribution of asperities within the wall surfaces could cause a local enhancement of permeability parallel to the DB/fault and negligible to the orthogonal direction. In consequence, the permeability is highly anisotropic allowing the fluid flow only parallel to the DB similar to a fracture.

Our results indicate that permeability depends on the different evaluated properties (i.e. effective porosity, specific surface area and tortuosity). Permeability is directly related to the effective porosity, and inversely related to the specific surface area and the tortuosity. In the case of DBs, where rock volumes are affected by cementation and cataclasis, the permeability obtained by the LBM differs to the K-C.

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