

# A high-voltage lithium-ion battery prepared using a Sn-decorated reduced graphene oxide anode and a $\text{LiNi}_{0.5}\text{Mn}_{1.5}\text{O}_4$ cathode

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**Abstract** This paper describes the preparation and characterization of a high-voltage lithium-ion battery based on Sn-decorated reduced graphene oxide and  $\text{LiNi}_{0.5}\text{Mn}_{1.5}\text{O}_4$  as the anode and cathode active materials, respectively. The Sn-decorated reduced graphene oxide is prepared using a microwave-assisted hydrothermal synthesis method followed by reduction at high temperature of a mixture of  $(\text{C}_6\text{H}_5)_2\text{SnCl}_2$  and graphene oxide. The so-obtained anode material is characterized by thermogravimetric analysis, X-ray diffraction, scanning electron microscopy, and electron diffraction spectroscopy. The  $\text{LiNi}_{0.5}\text{Mn}_{1.5}\text{O}_4$  is a commercially available product. The two materials are used to prepare composite electrodes, and their electrochemical properties are investigated by galvanostatic charge/discharge cycles at various current densities in lithium cells. The electrodes are then used to assemble a high-voltage lithium-ion cell, and the cell is tested to evaluate its performance as a function of discharge rate and cycle number.

**Keywords** Tin · Reduced graphene oxide ·  $\text{LiNi}_{0.5}\text{Mn}_{1.5}\text{O}_4$  · Composite electrodes · Lithium battery

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## Introduction

Lithium-ion batteries (LIBs) represent a milestone for the mobile power sources and are currently used for a large number of electrical applications. Nevertheless, the development of electric storage systems with higher performance requires the development of new electrode materials with higher specific capacity and/or higher voltage. At present, the attention is focused on high-voltage layered metal oxides for the cathode [1, 2] and high-capacity lithium storage metals and metal alloys for the anode [3]. The research activity on high-voltage cathode materials represents one of the key challenges for developing new advanced batteries with higher specific energies.  $\text{LiNi}_{0.5}\text{Mn}_{1.5}\text{O}_4$  (LNMO) with a spinel structure is emerging as one of the most promising active materials for the construction of high-energy Li-ion batteries [4–10]. This is mainly due to its high theoretical gravimetric specific capacity of  $146.7 \text{ mAh g}^{-1}$  coupled with a high working voltage (about 4.7 V below the Fermi energy of a lithium metal anode) leading to a theoretical gravimetric specific energy as high as  $650 \text{ Wh kg}^{-1}$  [10]. Due to the reduced nickel content in the material, the use of LNMO is also attractive from an economical point of view [11]. Lithium storage metals and alloys (intermetallics), such as Sn [12], Sb [13], Te [13], Al [14], Si [15], and SnSb [12], show high theoretical charge densities and impressive specific capacities and could replace the carbonaceous anode materials. Metallic Sn has a high theoretical capacity ( $993 \text{ mAh g}^{-1}$  or  $7262 \text{ mAh cm}^{-3}$  for  $\text{Li}_{4.4}\text{Sn}$ ) and a good electric conductivity. It also exhibits a moderate operating voltage that is useful to increase the safety of LIBs during rapid charge/discharge processes. These properties encourage the study of Sn as alternative anode material for high-performance LIBs [16]. Unfortunately, Sn maintains its good electrochemical characteristics for a little number of cycles and this behavior is caused by the disaggregation of the

electrode; it is possible to observe dramatic volume change (about 300 %) as a result of lithium-ion insertion/extraction. Sn nanostructures with metal organic framework [17], encapsulation of nanoparticles in carbon matrix [18], construction of hybrid anodes consisting of nanosized Sn and carbon [19], and dilution of the active material in a conductive matrix (e.g. the mixed-conductor matrix concept [20]) are proposed like possible solutions to improve the structural stability of the material and, consequently, the integrity of the Sn electrode. At the base of these strategies is the idea that low-dimension materials can better withstand the huge volume changes and that the conductive matrix can buffer the volume changes and increase the electrical conductivity of the active material, avoiding electric contact loss. Recently, graphite-based materials such as graphene oxide (GO), graphene, and chemically modified graphene oxides have received much attention for energy storage devices [21, 22]. The disadvantage of GO is the electrical insulation, increasing with the high presence of C–O bonds. The chemical reduction and the thermal annealing are commonly used to reduced GO, obtaining the electrically conducting reduced graphene oxide (RGO). RGO represents an excellent substrate to host active nanoparticles because of its intrinsically high conductivity, flexibility, large surface area, and chemical stability [23]. The chemical way to reducing GO involves the use of strong reducing agents, including hydrazine [24], hydroquinone [25], or  $\text{NaBH}_4$  [26]. Another proposed method requires the use of an acid solution added with metal powders (e.g., Fe and Al) [27, 28]. Alternatively, thermal annealing in  $\text{H}_2$  or mixture of  $\text{H}_2$  and Ar is reported to remove effectively the oxygen from the GO [29, 30]. Several techniques can be found in the literature to prepare Sn–graphene hybrids with various structures such as directly Sn-decorated graphene [31–34], Sn@C nanoparticles [35, 36], Sn@graphene [37–39], and sandwich-like graphene-supported hybrids [38–42]. Despite these hybrids have good electrochemical performances, at high charge/discharge rates, their cyclability is similar to other Sn carbon hybrid anodes. The poor rate performance of these Sn-based electrodes can be ascribed to four main factors: (i) the graphene nanosheets can regroup or stack irreversibly [43], (ii) the synthesis of RGO for exfoliation or reduction can introduce structural defects involving decreasing of stability and electronic conductivity [44], (iii) Sn nanoparticles do not always have the same size and are not equally distributed in the layers of graphene [45], and (iv) the graphene nanosheets not always have successful contact with adjacent Sn nanoparticles [46]. Moreover, the presence of nanostructures exposing active Sn can increase the irreversible capacity due to the direct contact with electrolyte causing possible side reactions at the interface [44]. Microwave-assisted hydrothermal synthesis method is also used for the preparation of  $\text{SnO}_2$ –graphene nanocomposites. Zhong et al. obtain materials with stable capacity [47], while Zhu et al. achieved  $\text{SnO}_2$ –graphene composites with

homogeneous distribution of tin oxide particles (100–200 nm) [48]. This preparation technique has many advantages with respect to conventional preparation methods such as fast heating and high efficiency. Microwave-assisted hydrothermal synthesis method is also used to impart novel structures and special morphologies to the active material for both anode and cathode [49, 50]. In this paper, we prepared a Sn–graphene composite to be used as an anode in LIB. The novelty of our approach consists in the preparation of a composite with a homogeneous size distribution of tin particles. This result is obtained using the microwave-assisted hydrothermal synthesis method. The Sn–graphene composite is obtained by heating a metal organic tin compound and GO in  $\text{H}_2/\text{Ar}$  atmosphere. The tin particles can reduce the irreversible aggregation of the graphene nanosheets, considered one of the causes of the capacity fade of the electrode. To reduce the problems related to unwanted side reactions between Sn and the electrolyte and to better control the size and distribution of Sn nanoparticles in the graphene layers, the amount of tin is kept very low. In order to enhance the electrode characteristics of the SnRGO electrode, we used a commercially available acrylic-styrene copolymer (Pattex PL50) as a binder. Pattex PL50 is a water-based dispersion of polystyrene acrylate (PSA) copolymer. In addition to the PSA copolymer, it contains some fillers and thickeners (mainly calcium carbonate). The PSA copolymer has a high chemical stability due to the absence of residual double bonds and a very high glass transition temperature, and consequently, the polymer film is very rigid. The chemical and physical characteristics that the polymer imparts to the resulting film are very good: high hydrophobicity, low water absorption, and great mechanical strength. In this paper, we present the synthesis and characterization of Sn-decorated RGO. The material is used to prepare an electrode tape using PSA copolymer as the binder, and the electrochemical properties of the electrode are tested at various charge/discharge rates. Finally, high-voltage lithium-ion battery is fabricated, coupling the SnRGO electrode with a LNMO-based cathode, and the electrochemical properties of the cells are studied as a function of current density and cycle number.

## Materials and methods

**Preparation of the Sn-decorated RGO** The synthesis procedure is detailed elsewhere [51]. Briefly, in a standard preparation, 0.5 g of GO (NanoInnova Technologies SL, Madrid) is dispersed by sonication in 50 ml of ethylene glycol (EG) until the formation of a stable suspension. 1.50 g of polyacrylic acid (PAA, MW ~2000; Sigma-Aldrich) is dispersed by sonication in about 20 ml of EG. A 0.05 M solution of phenyltin chloride [ $(\text{C}_6\text{H}_5)_2\text{SnCl}_2$ ] is prepared, dissolving 0.344 g of the salt in

about 20 ml of EG. The dispersion of PAA is added to the dispersion of GO dropwise, and the resulting suspension is allowed to sonicate for 2 h. The solution of phenyltin chloride is slowly added dropwise to the suspension of GO/PAA under vigorous stirring. The resulting mixture is sonicated for 2 h. The reaction mixture is placed in a microwave oven and irradiated with a power of 900 W for 10 min under stirring. The formed black solid is separated from the residual solution by filtration, washed three times with ethanol, and dried in air at 50 °C. The residue is processed in an oven at 800 °C in Ar/H<sub>2</sub> atmosphere (95:5) for 5 h and left to cool at room temperature.

**Preparation of the Sn-decorated RGO anode tape** 0.3 g of Sn-decorated RGO and 0.068 g of carbon black (Super P; MMM Carbon) are weighed and then transferred to a mill for the mixing. 0.032 g of Pattex PL50 (Henkel Düsseldorf, Germany) with a solid mass fraction of 90 % is dispersed in 5 g of water. The suspension is subsequently added to the powder mixture, and the components are mixed by operating the mill for a few minutes. The suspension that is thus obtained is used to paint a copper sheet covering a surface area of 100 cm<sup>2</sup>. After drying in air at 130–150 °C, the procedure is repeated as many times as it is necessary to use up the entire suspension. A typical negative electrode composition is 75.8 wt% SnRGO, 7.0 wt% Pattex PL50, and 17.2 wt% Super P. Electrodes are shaped to form a disc with a diameter of 12 mm and an average thickness of 40 μ. The electrode weight ranges from 2.0 to 2.5 mg, which corresponds to a specific mass loading of 1.76–2.21 mg cm<sup>-2</sup>. Lighter electrodes (from 0.9 to 1.1 mg with a specific mass loading of 0.68–0.83 mg cm<sup>-2</sup>) are obtained by punching the electrode tape in proximity of the edges. Prior to the electrochemical characterization, the electrodes are dried by heating under vacuum at 110 °C for 12 h.

**Preparation of the LNMO cathode tape** A procedure similar to that reported for the preparation of the anode tape is used to assemble the cathode. 0.75 g of LiNi<sub>0.5</sub>Mn<sub>1.5</sub>O<sub>4</sub> (Nanomyte SP-10; NEI Corporation Somerset, NJ, USA) and 0.10 g of carbon black (Super P; MMM Carbon, Belgium) are weighed and transferred to a mechanic mill. The powder is mixed by operating the device for a few minutes. A water dispersion of polyvinyl acetate (PVAc) with a solid mass fraction of 50 % is used (Vinavil SpA via Valtellina, 63-20159 Milan, Italy). 0.30 g of the PVAc dispersion is diluted with 8 g of water. The suspension of PVAc is added to the powder mixture and mixed by operating the mill for a few minutes. The so-obtained suspension is used to paint a thin aluminum sheet covering a surface area of 50 cm<sup>2</sup>. After drying in air at 130–150 °C, the procedure is repeated as many times as it is necessary to use up the entire suspension. The electrode composition is 75 wt% LiNi<sub>0.5</sub>Mn<sub>1.5</sub>O<sub>4</sub>, 15 wt% PVAc, and 10 wt% Super P. Electrodes are cut as discs, with a diameter of 12 mm

and a thickness of about 80 μ. The electrode weight ranged from 15.6 to 16.0 mg, which corresponds to a specific mass loading of 13.8–14.1 mg cm<sup>-2</sup>. Prior to the electrochemical characterization, the electrodes are dried by heating under vacuum at 110 °C for 12 h.

**Chemical-physical characterization** The morphology of the tapes is studied by scanning electron microscopy (SEM). High-magnification microphotographs are taken using an AURIGA, CrossBeam Workstation dual-column focused ion beam–SEM and a JEOL JSM-5510LV. The specimens are directly mounted onto a conductive double face carbon tape, which is previously mounted on a slab. The surface chemistry is mapped with an X-ray energy-dispersive spectroscopy (EDS) system (IXRF EDS-2000). The structure of the material is characterized by X-ray powder diffraction (XRD) analysis (Rigaku Miniflex) using Cu-Kα radiation. The thermal stabilities are investigated by the simultaneous use of a thermogravimetric (TG) and differential thermal analysis (DTA) instrument (Q600 SDT; TA Instruments) equipped with the Thermal Solution software (version 1.4). The reference for the calibration of temperature is nickel Curie point. Ceramic standard, furnished with instrument, permitted the mass calibration. An aluminum oxide with high grade of purity is used as a comparison material. The experiments are performed with open platinum crucibles (cross section=0.32 cm<sup>2</sup>) using 10–12 mg of samples. Starting from room temperature, the sample is heated with a gradient of 10 °C min<sup>-1</sup> up to 850 °C. The onset temperature is calculated by thermal analysis software (Universal Analysis, version 2.5) as the intersection between the extrapolated baseline and the tangent through the inflection point of the weight vs. temperature curve.

**Electrochemical characterization** For the electrochemical characterization, circular electrodes with a diameter of 12 mm are punched from the tape. Their electrochemical features are tested in a two-electrode lithium cell in which lithium acted both as the counter and reference electrode. The cells are set up by sandwiching a glass fiber, used as the separator, between the positive and the negative electrodes. The cycling performance and the cycle life of the cells are evaluated in 2032-type coin cells. A 1.0 M solution of LiPF<sub>6</sub> dissolved in EC/DEC (1:1) is used as the electrolyte. The cycling tests are automatically carried out with a battery cycler (Maccor 4000). All experimental activities are performed at 20 °C in a dry room (R.H. <0.1 % at 20 °C).

## Results and discussion

**Chemical–physical characterization of the Sn-decorated RGO** The thermal property of the SnRGO and the percentage of tin and carbon in the composite material are determined by

TG analysis, which is performed in air atmosphere with a heating rate of  $10\text{ }^{\circ}\text{C min}^{-1}$  from 20 to  $850\text{ }^{\circ}\text{C}$ . TGA measurement confirms the reduction of graphene oxide by the thermal treatment. In fact, as shown in Fig. 1, with the increasing of the temperature, the SnRGO shows no weight variations up to  $400\text{ }^{\circ}\text{C}$ , confirming a good thermal stability due to the absence of labile oxygen functional groups. A small weight loss occurs between  $420$  and  $550\text{ }^{\circ}\text{C}$ , which suggest the oxidation of graphene present on the surface of the SnRGO composite. After that, an important weight change occurs between  $550$  and  $650\text{ }^{\circ}\text{C}$ , which can reveal the oxidation of graphene present on the bulk of the composite material. The DTA shows a peak centered at  $625\text{ }^{\circ}\text{C}$ . With further heating, a little weight loss is observed for temperatures lower than  $750\text{ }^{\circ}\text{C}$ .

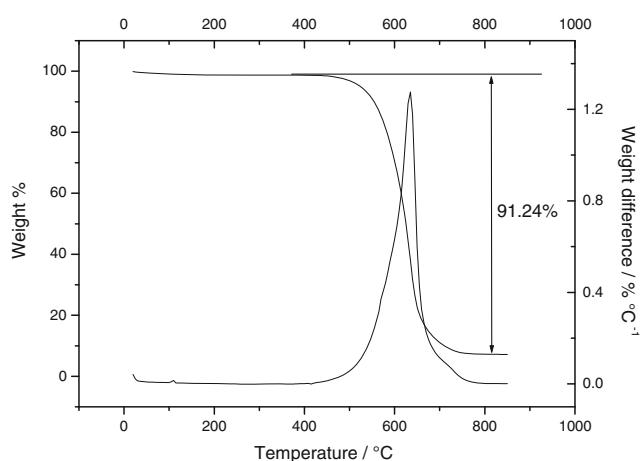
The weight percentage of the final residue is about  $8.76\text{ wt}\%$ . Considering that at elevated temperatures and in air the tin is completely converted into  $\text{SnO}_2$ , this value corresponds to the tin content in the composite (expressed as  $\text{SnO}_2$ ). Figure 2 shows the SEM image of the SnRGO composite material. It is possible to observe a fairly compact structure in which graphene layers are stacked and wrapped around each other, resembling a foliated graphite obtained by chemical flaking of natural graphite [52]. The porosity of the material is very high. The presence of spherical particles deposited on the surface of the graphite sheets is also noted. EDS analysis allowed to identify the chemical nature of the particles that results to the formation of tin. The Sn particles have a size ranging from  $200\text{ nm}$  up to  $400\text{ nm}$  and are highly dispersed on the RGO surface. The composite material appears rather uniform in size and shape; however, the particles are not homogeneously distributed on the graphene sheets. From EDS analysis, it is also possible to observe that the tin oxide produced by thermal decomposition of the organic precursor remains uniformly dispersed into the graphene matrix. On the other hand, metal tin tends to agglomerate forming the

spherical particles observed by SEM. This is probably due to the fact that the tin at the operative reduction temperature of  $800\text{ }^{\circ}\text{C}$  is in a liquid form.

XRD analysis (Fig. 3) gives further knowledge on the crystal structure and chemical structure of the tin present in the particles. All the peaks shown in Fig. 3 can be indexed as belonging to crystalline tin and tin oxide with a Cassiterite structure, as reported in the Joint Committee on Powder Diffraction Standards (JCPDS) card nos. 4-673 and 41-1445, respectively. The peak located at  $2\theta=30^{\circ}$  and indicated in Fig. 3 with an asterisk can be related to the presence of SnO with a Romachite structure (JCPDS card no. 6-395) that has the major reflection peak, corresponding to [010] plane, located at  $2\theta=29.96^{\circ}$ . The SnO can be originated by a partial reduction of  $\text{SnO}_2$  during the thermal annealing in  $\text{H}_2/\text{Ar}$  atmosphere. As regards the peak centered at about  $2\theta=26.6^{\circ}$ , it typically describes the formation of a RGO structure [53, 54], which tends to partially restack during the high-temperature treatment (graphene nanosheets).

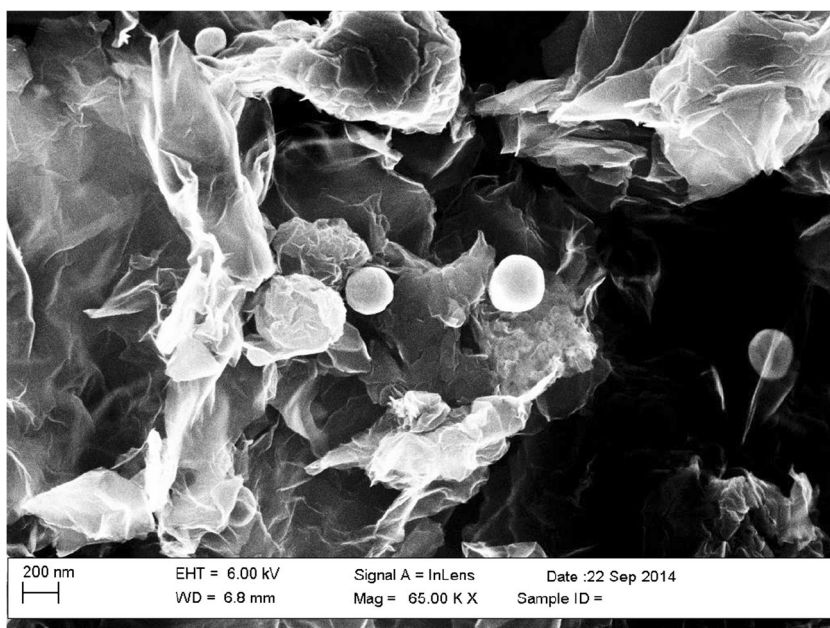
#### Chemical–physical characterization of the PSA–SnRGO tape

The TGA and the differential thermal gravimetry (DTG) profiles for the decomposition of the PSA–SnRGO tape in air are shown in Fig. 4. There is no mass loss up to  $200\text{ }^{\circ}\text{C}$ . By increasing the temperature, the thermal profile shows a behavior that can be related to the PSA depolymerization. This weight loss is related to the decomposition of oligomers with mostly head-to-head linking. A first peak, related to the PSA main-chain decomposition, can be observed in the DTG between  $230$  and  $435\text{ }^{\circ}\text{C}$  with a maximum centered at  $386\text{ }^{\circ}\text{C}$ . The decomposition temperature is comparable to that observed by Reza-Azimi et al. [55] for polystyrene methyl methacrylate. The total weight loss in this temperature range is about  $7.43\text{ wt}\%$ , higher than the percentage of binder into the electrode. This phenomenon could be imputed to the oxidation of the reactive graphene sheets present on the surface of the SnRGO, as previously observed for pure SnRGO. The main weight loss step occurs at temperatures ranging between  $400$  and  $580\text{ }^{\circ}\text{C}$  with a maximum centered at  $570\text{ }^{\circ}\text{C}$ . This step is assimilated to the oxidative degradation of the RGO. The total weight loss in this step is about  $62.6\text{ wt}\%$  (the theoretical weight loss in this step should be about  $64\text{ wt}\%$ ). It follows that not all the RGOs are burned in this temperature range. This finding is consistent with that found in the previous TGA for which the RGO is completely burned at temperatures above  $700\text{ }^{\circ}\text{C}$ . At the end of this degradation step, for temperatures higher than  $580\text{ }^{\circ}\text{C}$ , a third degradation step is observed. This step is shown as a shoulder in the down slope of the DTA curve. It can be related to the oxidative degradation of Super P carbon and the residual part of RGO. A final degradation step occurs for temperatures higher than  $625\text{ }^{\circ}\text{C}$ , and it is correlated to the decomposition of  $\text{CaCO}_3$  content as a filler into the Pattex 50 and the complete oxidation of the residual Super P



**Fig. 1** Thermogravimetric analysis for the SnRGO sample, carried out in air at a heating rate of  $10\text{ }^{\circ}\text{C min}^{-1}$

**Fig. 2** Scanning electron micrograph of the SnRGO sample

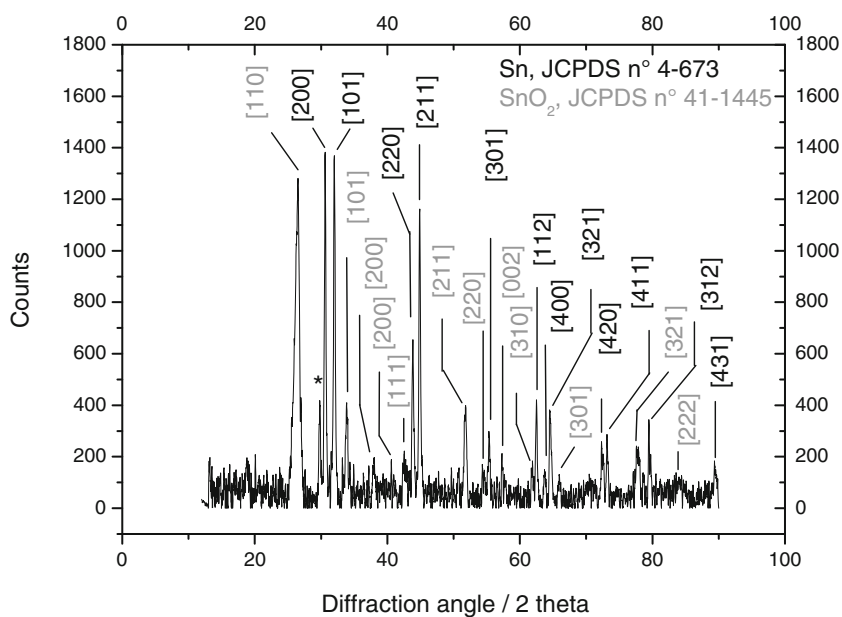


carbon and RGO still present in the sample. The total weight loss extending from 580 °C up to 690 °C amounts to 22.4 wt%. The residue of 7.79 wt% is formed by tin oxide and calcium oxide. Considering the percentage of Pattex 50 into the electrode (about 7.0 %), the percentage of  $\text{CaCO}_3$  in the Pattex 50 (about 50 %), and the percentage of weight loss due to the transformation of  $\text{CaCO}_3$  into  $\text{CaO}$  (46 %), the theoretical amount of  $\text{CaO}$  should be 1.61 wt%. By subtracting the percentage of  $\text{CaO}$  from the final residue, it is possible to obtain the percentage of  $\text{SnO}_2$  which amounts to 6.18 wt%. By dividing this value by the percentage of SnRGO in the composite tape (75.8 %), it is possible to calculate the percentage of tin (expressed as  $\text{SnO}_2$ ) into the SnRGO which amounts to

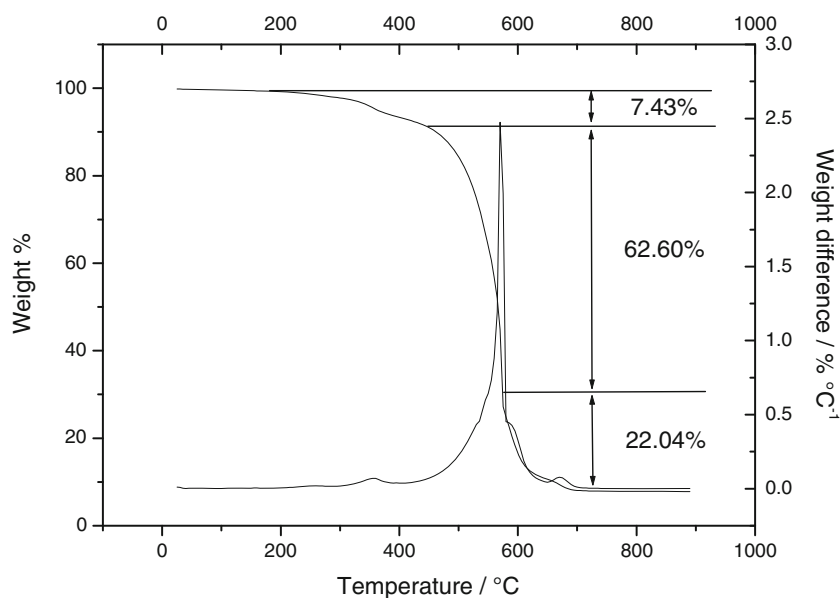
8.1 wt%, a value little bit lower than the previously obtained one (8.76 wt%).

The thickness and morphology of the electrode tape are investigated by SEM. Figure 5a shows the cross section of the electrode: it appears uniform with a thickness of about 55  $\mu\text{m}$ . Figure 5b shows the low-magnification image of the anode surface ( $\times 100$ ). The surface depicted in the figure has an area of about 0.9  $\text{mm}^2$ . Although the surface is quite smooth, some rough edges emerge from the plane. On the other hand, it is also possible to note the presence of some holes and cracks. The parts that emerge from the surface of the electrode as well as the electrode cracks can be directly related to the deposition process (in which a brush is used for the

**Fig. 3** XRD patterns of the SnRGO sample. The diffraction planes for Sn and  $\text{SnO}_2$  are reported in *black* and in *gray*, respectively



**Fig. 4** Thermogravimetric analysis for the PSA–SnRGO electrode tape, carried out in air at a heating rate of  $10\text{ }^{\circ}\text{C min}^{-1}$



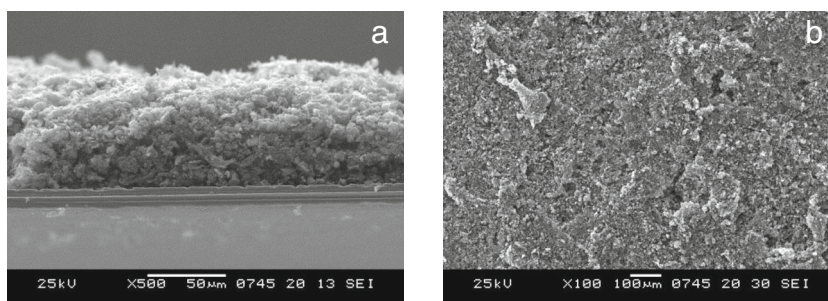
coating of the current collector). The holes are probably formed during the drying phase due to the release of vapor bubbles in which evaporation leaves empty spaces in the tape electrode.

X-ray EDS is performed in order to evaluate the homogeneity and distribution at a microscopic level of the various components within the electrode. The distribution of carbon, oxygen, calcium, and tin is investigated inside the thickness of the electrode. The correspondent distribution maps are depicted in Fig. 6. The carbon appears uniformly distributed on the whole thickness of the electrode. The oxygen content appears very low. This is probably due to the fact that oxygen is present only as  $\text{SnO}_2$  or  $\text{CaCO}_3$ . Calcium is mapped as a marker to evaluate the uniformity of the binder distribution into the electrode, and it has very good results. Also, the signal of Sn is equally distributed into the electrode, confirming the uniformity of the electrode and the validity of the covering method to obtain an almost homogeneous electrode.

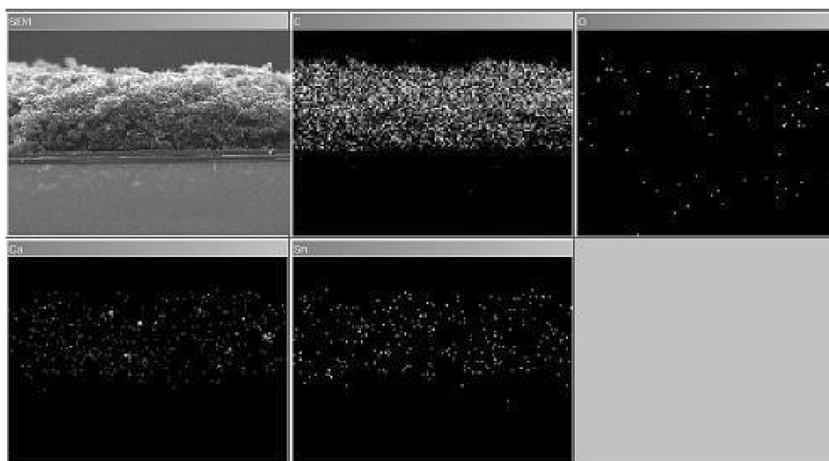
**Electrochemical characterization** Figure 7a shows the first charge/discharge voltage profile for the PSA–SnRGO electrode. The active material in the electrode weighs 1.0 mg.

The electrode is cycled at a specific current of  $100\text{ mA g}^{-1}$  between 2.0 and 0.01 V. During the first lithiation cycle, the electrode is able to accommodate about  $600\text{ mAh g}^{-1}$ . Only part of the capacity accumulated in the first discharge can be extracted from the electrode. In fact, in the following charge, the electrode is able to restore only  $380\text{ mAh g}^{-1}$ . The irreversible capacity in the first cycle corresponds to about 37%. As reported by other authors, this irreversible capacity is caused by the degradation of the electrolyte and by the formation of a passivation layer on the electrode surface. Also, the reduction of  $\text{SnO}_2$  to Sn contributes to the irreversible capacity [51] being, as demonstrated by XRD analysis, the metal oxide still present in the composite after the thermal treatment under reducing atmosphere. The first-cycle irreversible capacity, and the following reversible charge behavior of the SnRGO electrode, can be better explained by analyzing the differential capacity curve shown in Fig. 7b. The differential capacity ( $Q_{\text{diff}}$ ), given by  $Q_{\text{diff}} = [d(\text{mAh})/d(\text{V})]$ , is the derivative of the amount of charge added (charge cycle) or charge removed (discharge cycle) with respect to the cell voltage. The differential profile of the first discharge shows a large amount of capacity exchanged by irreversible processes in the voltage

**Fig. 5** Scanning electron micrographs of the PSA–SnRGO electrode tape deposited on a copper current collector. **a** High-magnification image ( $\times 500$ ) of the electrode cross section. **b** Low-magnification image ( $\times 100$ ) of the electrode surface

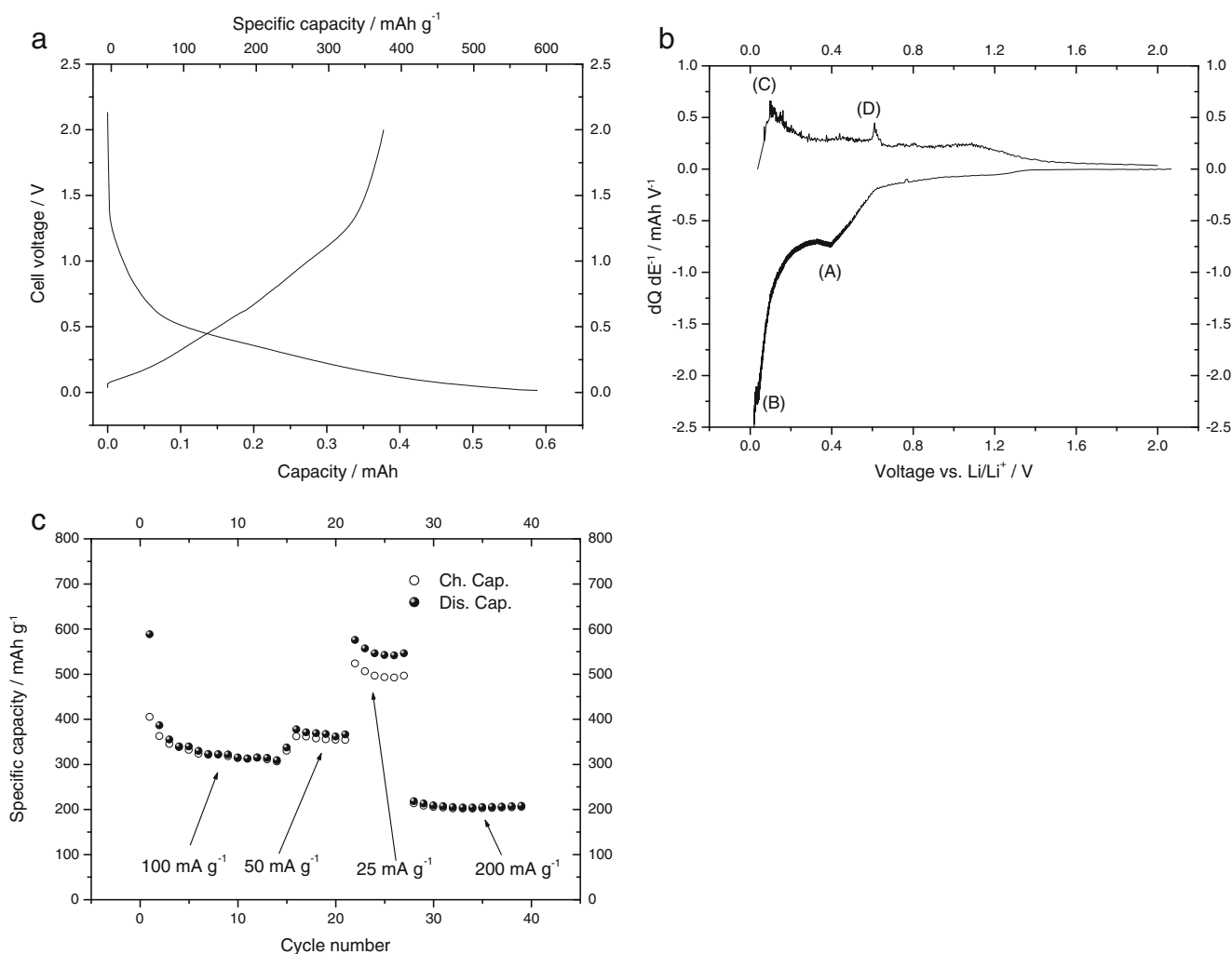


**Fig. 6** Distribution maps of the PSA-SnRGO electrode cross section for carbon, oxygen, calcium, and tin as obtained by X-ray energy-dispersive spectroscopy



range 0.6 to 0.3 V, with a peak centered at 0.4 V (A). This can be mainly ascribed to the formation of a solid electrolyte

interphase (SEI) between the electrolyte and the active material, taking place preferentially at the surface of RGO



**Fig. 7** **a** First-cycle voltage profile as a function of the capacity for a PSA-SnRGO electrode cycled in a lithium cell at 100 mA g<sup>-1</sup>. **b** Differential  $dQdE^{-1}$  vs.  $E$  curves corresponding to the voltage profiles shown in **a**. **c** Specific capacity (in charge and discharge) and Coulombic efficiency

as a function of the number of cycles at various charge/discharge currents. The weight of the electrode active material is 0.98 mg. The active material load for unit area is 0.86 mg cm<sup>2</sup>

nanosheets and with the SnO<sub>2</sub> reduction. The formation of the SEI is the main reason for the very large irreversible capacity, which is commonly evidenced for composite materials where an amorphous carbon matrix is the main component of the active material [56, 57], as in the case for the SnRGO composite under investigation. Further irreversible capacity can be ascribed to Li storage at the surface, cavities, and defects of the disordered carbon [58, 59]. Below 0.3 V, a high and relatively broad peak shows up (B), corresponding to the sloping plateau in Fig. 7a at the same potential values. This feature can be associated mainly with Li intercalation into the partly restacked RGO matrix and, partially, to the Sn lithiation. In the subsequent charge, a couple of peaks are observed: a large one (C) at 0.1 V followed by a smaller peak (D) centered at 0.6 V. It is noteworthy that Li extraction still continues to the higher potential and it is completed only at voltages higher than 1.0 V. The first peak (C) can be ascribed to reversible Li de-intercalation from the RGO, and it accounts for a large part of the reversible capacity. The second peak observed at 0.6 V and the remaining capacity extracted at voltages between 0.5 and 0.9 V can be attributed to lithium de-alloying from Li<sub>x</sub>Sn [60].

Figure 7c shows the specific capacity (both in charge and discharge) and the Coulombic efficiency as a function of the number of cycles at various charge/discharge currents. By analyzing Fig. 7c, it is possible to note that the irreversible capacity is not limited to the first cycle but this phenomenon also affects the subsequent cycles. In fact, also if in a reduced manner, the specific capacity in discharge (filled circle in Fig. 7c) is larger than the specific capacity in charge (hollow circle in Fig. 7c). After the 4th cycle, the capacities in charge and discharge assume a similar value and the charge coefficient reaches a unitary value. It is important to highlight that increasing the charge/discharge rate, the irreversible capacity decreases. In fact below 50 mA g<sup>-1</sup>, the difference between the capacity in charge and discharge increases and this effect is boosted when the cycling rate is further decreased down to 25 mA g<sup>-1</sup>. Contrarily, the reversibility of the insertion/de-insertion process is perfectly restored when the cycling rate is increased up to 200 mA g<sup>-1</sup>. This behavior can be explained assuming that the kinetics of the lithium insertion process into the material is larger than that of the parasitic reaction responsible of the irreversible capacity. If this hypothesis is respected, at high charge/discharge rate, the main phenomenon occurring at the electrode is the lithium intercalation in RGO while at low cycling rate, both phenomena can occur, determining a decrease of the efficiency of the process. Figure 8a shows the relation between the capacity (and specific capacity) at the various cycling rates with the voltage trend. At the lowest rate (25 mA g<sup>-1</sup>), a specific capacity approaching 460 mAh g<sup>-1</sup> is obtained. By doubling the specific current, the capacity decreases to about 320 mAh g<sup>-1</sup>. For further doubling of the specific current, the capacity decreases

to about 280 mAh g<sup>-1</sup>. A more remarkable capacity decrease is observed when charging the electrode at 200 mA g<sup>-1</sup>: the specific capacity goes down to 202 mAh g<sup>-1</sup>.

To establish the discharge performance of the SnRGO electrode at different current densities, Peukert dependence is measured. The Peukert law is presented by Eq. (1) [61]:

$$C_r = T_{\text{dis}} I_{\text{dis}}^k \quad (1)$$

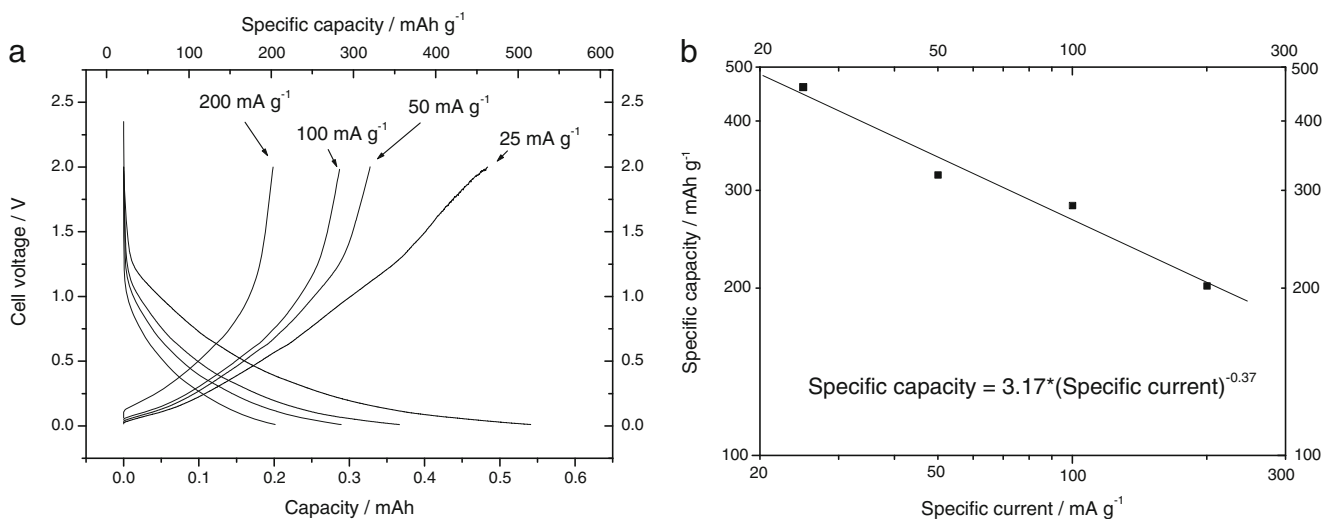
where  $C_r$  represents the rated discharge capacity in (mAh) and  $T_{\text{dis}}$  and  $I_{\text{dis}}$  are the discharge time and discharge current expressed in hours and milliamperes, respectively. The  $k$  parameter is the Peukert constant. The Peukert constant provides an indication of the power capability of the cell: the smaller the value of  $k$ , the higher the power capability. This parameter is strongly dependent on the battery technology: for lithium-ion technology, this parameter changes between 1.00 and 1.28 [62]. The effective capacity ( $C_e$ ) is the product of the discharge time and discharge current. By rearranging Eq. (1), we can obtain Eq. (2) in which the effective capacity ( $C_e$ ) is related to the rated discharge capacity ( $C_r$ ), Peukert constant ( $k$ ), and discharge current ( $I_{\text{dis}}$ )

$$C_e = T_{\text{dis}} I_{\text{dis}} = C_r I_{\text{dis}}^{1-k} \quad (2)$$

To evaluate the Peukert constant ( $k$ ), the specific discharge capacity is plotted as a function of the specific current in a double logarithmic plot as shown in Fig. 8b. From the slope of the curve, a Peukert constant ( $k$ ) of 1.37 is calculated.

Once the PSA-SnRGO electrode is electrochemically characterized and before to use the electrode as an anode in a full LIB cell, the electrochemical behavior of the cathode tape is investigated and Fig. 9a shows the discharge voltage trend for the PVAc-LNMO electrode. To quantify the consequence of the lithiation rate on the specific capacity, the electrode is cycled between 4.85 and 3.0 V at different currents corresponding to the discharge rates of C/10, C/5, C, 2C, and 3C. The charge is performed galvanostatically at C/10 rate up to 4.85 V. The specific capacity based on the weight of the active material in the electrodes varies with the discharge current. A maximum value of 123 mAh g<sup>-1</sup> is obtained by discharging the electrode at 13 mA g<sup>-1</sup>. By increasing the specific discharge current, the specific capacity decreases but the capacity retention is fairly good: the electrode is able to discharge about 93 % of the C/10 capacity when discharged at specific current 10 times higher and about 86 % of the C/10 capacity when discharged at currents 30 times higher. The correlation between the electrode performance and the discharge current is better shown in Fig. 9b, reporting in a double logarithmic plot the specific capacity as a function of the specific discharge current. Also, in this case, a linear behavior is observed. The  $k$  parameter is evaluated to be 1.037. The low value of the  $k$  parameter is probably related to the nanometric

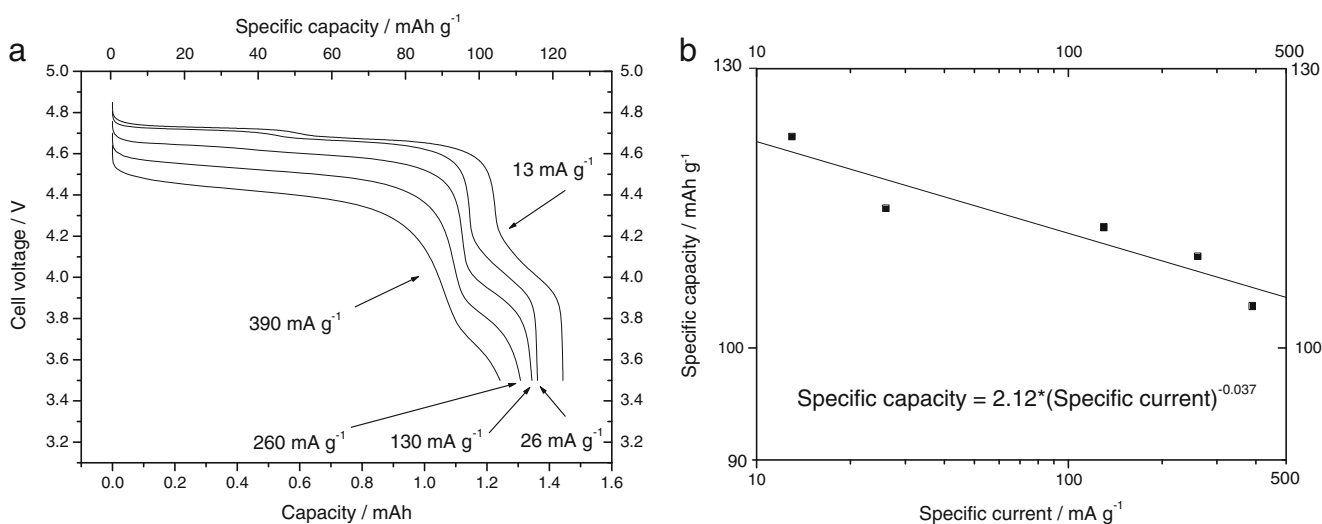




**Fig. 8** **a** Voltage profiles as a function of the capacity for the electrode described in Fig. 7 cycled at various discharge rates. **b** Double logarithmic plot reporting the specific capacity as a function of the specific current

size of the LNMO that allows to cycle the electrode with good utilization at every discharge rate. Once the electrochemical properties of the positive electrode are evaluated, a full lithium-ion battery cell is built by coupling the PSA–SnRGO and the PVAc–LNMO electrodes. The characteristics of the positive and negative electrodes used to assemble the lithium-ion battery cell are reported in Table 1. The battery is perfectly balanced with the ratio between the anode and cathode capacity being equal to 1.0. An initial electrochemical test is carried out by cycling the battery at 0.2 mA. Two end conditions are set in charge regarding the maximum charging capacity (1.0 mAh) and the maximum allowed voltage (4.95 V). The battery is discharged at the same current down to 2.0 V. Figure 10a shows the charge/discharge voltage profiles for the cell. In the first two charge cycles, the cell is able

to charge the maximum amount of allowed capacity (1.0 mAh) without reaching the end voltage condition. Starting from the third cycle, the charge is stopped because the cell reaches the end voltage condition. In the first discharge, only a part of the capacity inserted into the electrode is discharged (about 0.34 mAh). The irreversible first-cycle capacity is about 66 %. The high value of the irreversible capacity is due to the fact that during the first cycle, the cell is not completely charged. After the second cycle, the cell is almost completely charged and the discharge capacity increases to 0.65 mA. The second-cycle discharge capacity is about 76 % of the capacity in charge. During the second cycle, the discharge capacity increased because the irreversible capacity is almost completely consumed during the previous charge cycle. At the third cycle, the cell discharges the



**Fig. 9** **a** Voltage profiles as a function of the capacity for a PVAc–LNMO electrode cycled in a lithium cell at various discharge currents. **b** Double logarithmic plot reporting the specific capacity as a function of the

specific current. The weight of the electrode active material is 11.7 mg. The active material load for unit area is 10.35 mg cm<sup>2</sup>

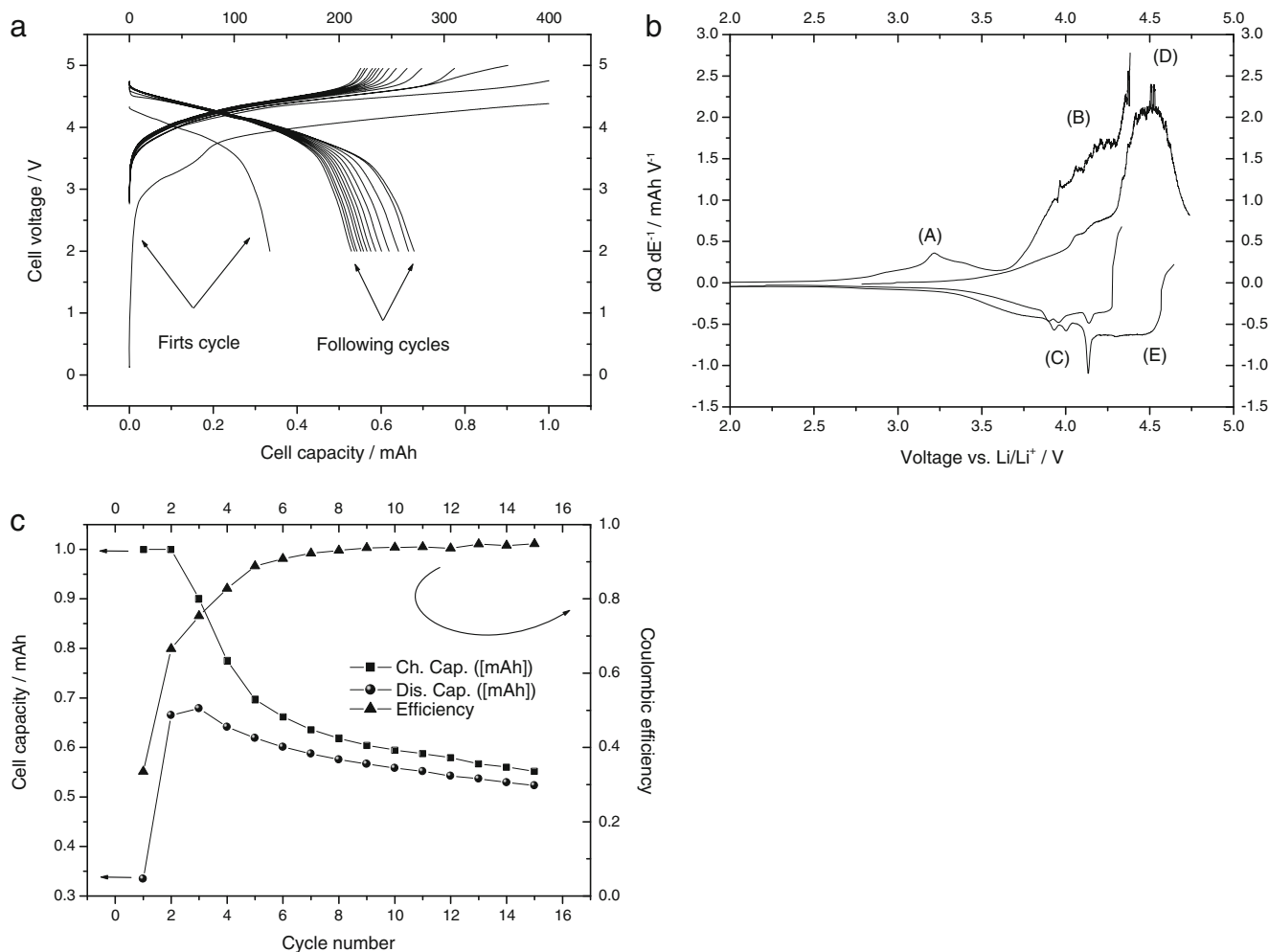
**Table 1** Characteristics of the positive and negative electrodes used to assemble the lithium-ion battery cell. To calculate the first-cycle capacity, a specific capacity of 588 and 123 mAh g<sup>-1</sup> is used for the SnRGO and

the LNMO, respectively. To calculate the reversible capacity of the cell, a specific capacity of 300 mAh g<sup>-1</sup> is used for the SnRGO electrode

Electrode	Electrode weight, mg	Active material weight, mg	First-cycle electrode capacity, mAh	Capacity ratio	Reversible electrode capacity (at 100 mA g <sup>-1</sup> ), mAh
C (+)	16.0	12.0	1.476	1.00	—
A (-)	3.3	2.5	1.470	0.99	0.75

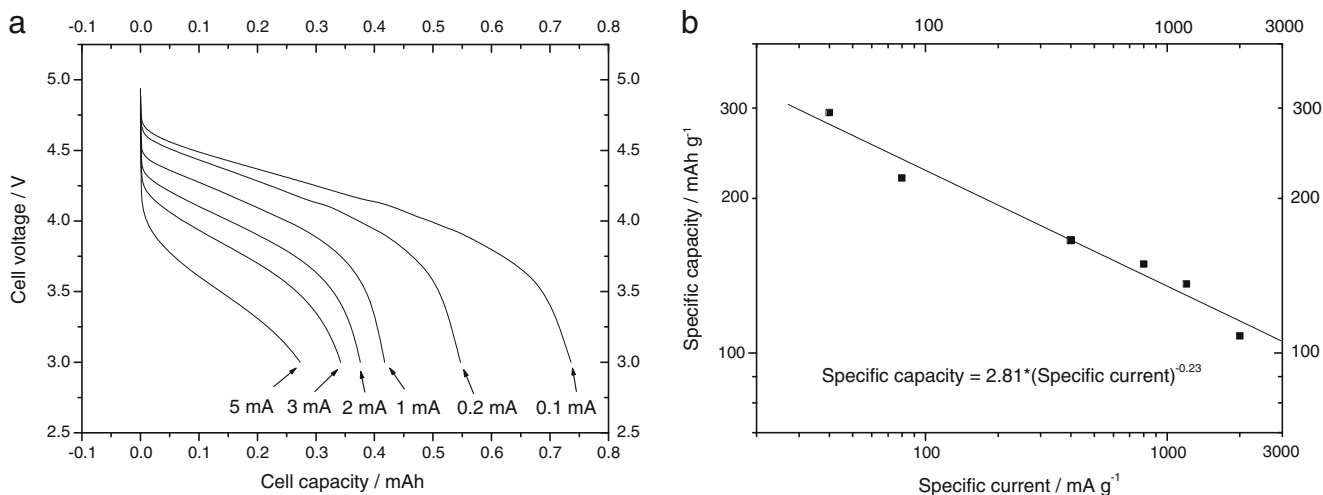
maximum capacity (about 0.68 mAh). The discharge processes in the following cycles are all similar to each other as regard the voltage profiles but differ in that the capacity tends to decrease with the progress of the number of cycles. To illustrate the origin of the first-cycle irreversible capacity and the better reversible charge/discharge behavior exhibited at the second cycle, the calculated  $dQ/dE^{-1}$  vs.  $V$  differential profiles for the 2 cycles is shown in Fig. 10b. The differential profile of the first charge shows an amount of capacity exchanged by an

irreversible process in the voltage range 2.5 to 3.5 V (A). A further source of irreversible capacity can be observed between 3.7 and 4.3 V (B). Process A is completely irreversible because it disappears during the second charge step, while process B is partially reversible because a part of it is also observed during the second charge step. A third charge process started just after 4.3 V, but it is stopped because the cell reached one of the end charge conditions (the maximum charge capacity is set to 1.0 mAh). In the first discharge step,



**Fig. 10** a Voltage profiles for the first 15 cycles as a function of the capacity for a PVAc-LNMO/PSA-SnRGO Li-ion battery cell cycled at 0.2 mA. b Differential  $dQ/dE^{-1}$  vs.  $E$  curves corresponding to the voltage profiles shown in a. c Capacity (in charge and discharge) and charge

coefficient as a function of the number of cycles. The weights of the electrode active materials for the cathode and the anode are 12.0 and 2.5 mg, respectively. The active material loads for unit area for the cathode and the anode are 10.61 and 2.21 mg cm<sup>2</sup>, respectively

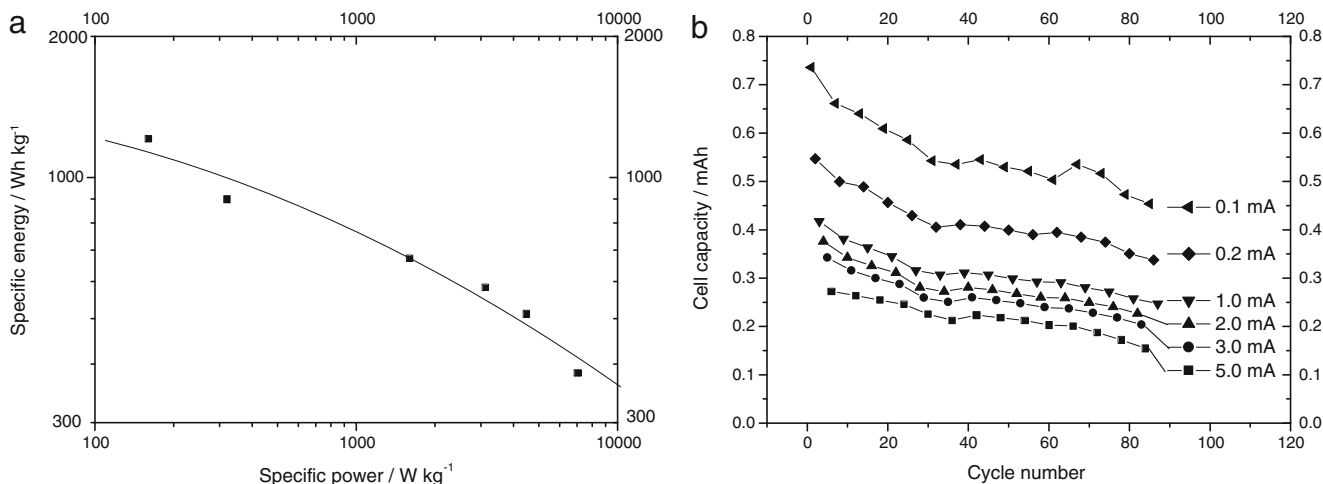


**Fig. 11** a Voltage profiles as a function of the capacity for the Li-ion battery cell described in fig. 10 cycled at various discharge currents (the current values are reported in the figure). b Double logarithmic plot

reporting the specific capacity as a function of the specific discharge current

the accumulated capacity is released between 4.3 and 3.3 V (C). In this voltage range, it is possible to observe three peaks located at 4.14, 3.95, and 3.90 V. These peaks are also observable during the second discharge step although with a small shift with respect to the previous cycle. During the second charge step, process B is strongly reduced in intensity while a large capacity is accumulated between 4.3 and 4.7 V (D) with a peak centered at 4.5 V. In the second discharge step, a correspondent reduction wave is observed between 4.6 and 4.3 V (E). The cycle life of the cell can be observed in Fig. 10b where the capacity in charge and discharge is related to the cycle number. In the same figure, the charge coefficient (right axis) is also reported. As previously described, the discharge capacity increases during the first 3 cycles, taking up to 0.68 mAh, and then slowly decreases. At the same time also, the charge capacity decreases so that the Coulombic efficiency

increases with the progress of the number of cycles, rising to 0.95 at the 15th cycle. At this point, the capacity is reduced down to 0.52 mAh. In order to estimate the effect of the discharge rate on the capacity, the cell is cycled at various current densities. The charge is performed galvanostatically at 0.1 mA up to 4.95 V. Figure 11a shows the voltage behavior of the LIB cell. When discharged at the lower discharge rate (0.1 mA), the battery is able to provide the theoretical reversible capacity (0.75 mAh). By increasing the discharge current, a decrease in the specific capacity and in the average discharge voltage is observed. The specific capacity decreases to about 0.54 mAh by doubling the current; at 0.41 mAh, by increasing the discharge current of 10 times; and at 0.27 mAh, by increasing the discharge rate on the performance of the material is summarized in Fig. 11b in which the specific capacity is reported as a function of the



**Fig. 12** a Double logarithmic plot of the specific energy as a function of the specific power (Ragone plot). The specific values are referred to the weight of the active material in the anode. b Discharge capacity as a

function of the number of cycle number for the Li-ion battery cell described in Fig. 10 cycled at various discharge rates

specific discharge current in a double logarithmic plot (both the specific values are referred to the weight of the active material in the anode electrode). A linear behavior is observed between the discharge current and the cell capacity: from the slope of the linear interpolation fit, a value of 1.23 is found for the  $k$  parameter. This value is slightly lower than the value found for the PSA–SnRGO electrode, and it confirms that the kinetic of the lithium-ion battery cell is anode limited. The effect of the discharge rate on the performance of the material is summarized in the Ragone plot depicted in Fig. 12a in which the specific energy is reported as a function of the specific power in a double logarithmic plot. The specific values are referred to the weight of the active material in the anode. The Ragone plot shows that at low power, the specific energy is about 1210 Wh kg<sup>-1</sup> and it is reduced at about 383 Wh kg<sup>-1</sup> when the cell is discharged at a specific power in excess of 7000 W kg<sup>-1</sup>. The cyclability of the lithium-ion battery cell is shown in Fig. 12b where the specific capacity is plotted as a function of the cycle number. The capacity fading is pronounced and ranges between 0.5 and 0.55 % per cycle as a function of the discharge rate.

## Conclusions

In this paper, we studied the electrochemical performance of a high-voltage lithium-ion battery cell using Sn-decorated RGO and LNMO as the anode and the cathode, respectively. Microwave-assisted hydrothermal synthesis method allowed to prepare a Sn-decorated GO composite material. As confirmed by XRD analysis and TGA measurement, the GO is almost completely reduced by thermal annealing in H<sub>2</sub>/Ar atmosphere while the SnO<sub>2</sub> is only partially reduced. The tin content in the composite expressed as SnO<sub>2</sub> is 8.76 wt%. The material presents a compact structure in which graphene layers are stacked and wrapped around each other with spherical tin-based particles deposited on the surface of the graphene sheets. The tin-based particles have a size ranging from 200 nm up to 400 nm and are highly dispersed on the RGO surface. An electrode tape with a thickness of about 55 μm is obtained using a commercially available acrylic–styrene copolymer (Pattex PL50). The so-obtained electrode tape shows a good homogeneity between the various chemical elements constituting the electrode. The electrode surface appears rough due to the presence of edges, holes, and cracks. The electrode is found stable up to 200 °C, and it starts to decompose at 230 °C. The electrochemical characterization shows that a large irreversible capacity affects the electrode. This irreversible capacity is related to the degradation of the electrolyte, to the formation of a passivation layer on the electrode surface, and to the reduction of SnO<sub>2</sub> to Sn. The irreversible capacity is not limited to the first cycle, but it also affects the subsequent cycles. Furthermore, the irreversible

capacity increases by decreasing the charge/discharge rate. This behavior is explained considering the faster kinetics of the lithium insertion into the material with respect to the kinetics of the parasitic reaction responsible of the irreversible capacity. The positive electrode of the lithium-ion battery is prepared using a procedure similar to that reported for the preparation of the anode and using PVAc as the binder. The electrochemical performance of both the electrodes is evaluated at various current densities. The Peukert constant is calculated for both the electrodes to characterize the system response in power. It results that the positive electrode is more performing in power with respect to the negative one. The good response exhibited by the positive electrode is related to the nanometric size of the LNMO used for the preparation of the electrode. The electrochemical performance of the full lithium-ion battery cell built by coupling the PSA–SnRGO and the PVAc–LNMO electrodes is found corresponding to the expectations. In the first lithiation cycle, due to the large first-cycle irreversible capacity, only 34 % of the capacity inserted into the electrode is discharged. The irreversible capacity decreases in the following cycles and the Coulombic efficiency increases rising to 0.95 at the 15th cycle. When discharged at the lower discharge current, the battery is able to provide its theoretical reversible capacity (0.75 mAh). The specific capacity decreases to about 0.41 mAh by increasing the discharge current of 10 times and to 0.27 mAh by increasing the discharge current of 50 times. A value of 1.23 is found for the Peukert constant. This value is slightly lower than the value found for the PSA–SnRGO anode electrode (1.37), and it confirms that the kinetics of the lithium-ion battery cell is anode limited. The Ragone plot shows that at low power, the specific energy, based on the weight of the active material in the negative electrode, is about 1210 Wh kg<sup>-1</sup> and it reduces at about 383 Wh kg<sup>-1</sup> when the cell is discharged at a specific power in excess of 7000 W kg<sup>-1</sup>. Relatively high capacity fading affects the cell performance with the progress of the cycle number. The capacity fading ranges between 0.5 and 0.55 % per cycle as a function of the discharge rate.

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